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Sir:

Enclosed for filing is the patent application of:

Inventors: Philip R. Jeffs and Dennis A. Bohn

Title: IMPROVED TONE-CONTROL CIRCUIT AND METHOD FOR
CONDITIONING RESPECTIVE FREQUENCY BANDS OF AN AUDIO
SIGNAL

Including:

- X 1. A specification including claims consisting of 50 pages.
- X 2. Drawings consisting of 25 sheets.
- X 3. Declaration and Power of Attorney.

Additionally:

- X 4. An assignment of the invention to Rane Corporation is attached.
- X 5. A Verified Statement Claiming Small Entity Status is enclosed.
- X 6. A filing date in accordance with 37 CFR 1.10 is requested
(Express mail certificate is part of this transmittal letter).

X 7. COMPUTATION OF FEE

	Number Filed	Number Extra		Basic Fee
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- X 8. Check No. 13864 for \$950.00 for filing fee is enclosed.
X 9. Check No. 13865 for \$40.00 for assignment fee is enclosed.
___ 10. No fee is enclosed at this time.
X 11. Charge any additional fees to Deposit Account No. 07-1897.
X 12. A copy of this letter is enclosed.
X 13. A postcard is enclosed as acknowledgment of receipt of this application.

Respectfully submitted,

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Filed or Issued: _____

For: IMPROVED TONE-CONTROL CIRCUIT AND METHOD FOR CONDITIONING
RESPECTIVE FREQUENCY BANDS OF AN AUDIO SIGNAL

**VERIFIED STATEMENT (DECLARATION) CLAIMING SMALL ENTITY STATUS
(37 CFR 1.9(f) AND 1.27(c)) - SMALL BUSINESS CONCERN**

I hereby declare that I am

- ☐ the owner of the small business concern identified below:
- ☒ an official of the small business concern empowered to act on behalf of the concern identified below:

NAME OF CONCERN Rane Corporation

ADDRESS OF CONCERN 10802 47th Avenue West

Mukilteo, Washington 98275-5098

I hereby declare that the above-identified small business qualifies as a small business concern as defined in 13 CFR 121.3-18, and reproduced in 37 CFR 1.9(d), for purposes of paying reduced fees under Section 41(a) and (b) of Title 35, United States Code, in that the number of employees of the concern, including those of its affiliates, does not exceed 500 persons. For purposes of this statement, (1) the number of employees of the business concern is the average over the previous fiscal year of the concern of the persons employed on a full-time, part-time or temporary basis during each of the pay periods of the fiscal year, and (2) concerns are affiliates of each other when either, directly or indirectly, one concern controls or has the power to control the other, or a third party of parties controls or has the power to control both.

I hereby declare that rights under contract or law have been conveyed to and remain with the small business concern identified above with regard to the invention described in

- ☒ the specification filed herewith with the title as listed above.
- ☐ the application identified above.
- ☐ the patent identified above.

If the rights held by the above-identified small business concern are not exclusive, each individual, concern or organization having rights to the invention is listed below* and no rights to the invention are held by any person, other than the inventor, who could not qualify as a small business concern under 37 CFR 1.9(d) or by any concern which would not qualify as a small business concern under 37 CFR 1.9(d) or a nonprofit organization under 37 CFR 1.9(e).

*NOTE: Separate verified statements are required from each named person, concern or organization having rights to the invention averring to their status as small entities. (37 CFR 1.27).

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☐ INDIVIDUAL ☐ SMALL BUSINESS CONCERN ☐ NONPROFIT ORGANIZATION

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I acknowledge the duty to file, in this application or patent, notification of any change in status resulting in loss of entitlement to small entity status prior to paying, or at the time of paying, the earliest of the issue fee or any maintenance fee due after the date on which status as a small entity is no longer appropriate. (37 CFR 1.28(b)).

I hereby declare that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under Section 1001 of Title 18 of the United States Code, and that such willful false statements may jeopardize the validity of the application, any patent issuing thereon, or any patent to which this verified statement is directed.

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IMPROVED TONE-CONTROL CIRCUIT AND METHOD FOR CONDITIONING RESPECTIVE FREQUENCY BANDS OF AN AUDIO SIGNAL

Technical Field:

5 The invention relates generally to electronic circuits, and more particularly, to an improved tone-control circuit and method for controlling the gains of one or more of the bass, mid, and treble frequency bands of an audio signal.

Background of the Invention:

10 Within the last few years, the music world has witnessed the birth and increasing popularity of a new type of composer/performer known as a "turntablist". Generally, a turntablist performs a musical piece by manually rotating one or more conventional phonographic records to generate musical sounds.

15 Figure 1 is a schematic block diagram of a conventional sound system 10 that is used by many of today's turntablists. The system 10 includes a pair of turntables 12 and 14, which amplify the sounds from respective phonographic records 13 and 15. The turntables 12 and 14 respectively provide first (PGM1) and second (PGM2) program audio signals to an audio mixer 16, which mixes these signals together to generate a mixed master audio signal (MASTER). An optional effects box 18
20 generates a signal (MASTER EFFECTS) by adding audio effects to the MASTER signal. Typically, the PGM1, PGM2, MASTER, and MASTER EFFECTS signals are stereo signals having respective left (L) and right (R) components. A house amplifier 20 amplifies the MASTER EFFECTS signal and provides its L and R components to speakers 22 and 24, respectively.

25 Figure 2 is a control panel 26 of the mixer 16 of Figure 1. The mixer 16 includes gain controls 28 and 30 for respectively adjusting the gains of the PGM1 and PGM2 signals (Figure 1) over their entire frequency ranges, bass controls 32 and 34 for respectively adjusting the gains of the low-frequency components of PGM1 and PGM2, and treble controls 36 and 38 for respectively adjusting the gains
30 of the high-frequency components of PGM1 and PGM2. Because the turntables 12 and 14 (Figure 1) may provide PGM1 and PGM2 with different gains, the controls 28 and 30 allow the turntablist to compensate for these gain differences so that PGM1 and PGM2 have the same amplitude characteristics before the mixer 16 processes

them further. Additionally, the turntablist may set the controls 32, 34, 36, and 38 to attenuate or amplify the bass or treble-bands of PGM1 and PGM2, respectively. For example, the turntablist may want to isolate a singing voice from the record 13.

Because the frequency components of a human voice lie mainly in the mid band
5 between the bass and treble-bands, the turntablist adjusts the controls 32 and 36 for full attenuation, *i.e.*, "cut", so that ideally only the mid-band frequency components of PGM1 are audible in the MASTER EFFECTS signal (or the MASTER signal if the effects box 18 is not included in the system 10).

The mixer 16 also includes input-fader controls 40 and 42 for adjusting the
10 volumes of PGM1 and PGM2 — as heard in the MASTER signal — after PGM1 and PGM2 have been processed by the amplification circuitry controlled by the controls 28, 30, 32, 34, 36, and 38. Typically, the fader controls 40 and 42 are respective sliding controls, such as sliding potentiometers, that the turntablist uses to vary the respective volumes of PGM1 and PGM2 for musical effect while he is playing his
15 piece.

Figure 3 is a plot of a curve 43, which shows the attenuation in decibels (dB)
of PGM1 and PGM2 versus the control position for a known version of the input-fader controls 40 and 42, respectively, of Figure 2. For clarity here and below, the characteristics and operation of the control 40 are discussed, it being understood
20 that the characteristics and operation of the control 42 are similar. In operation, referring to both Figures 2 and 3, if the control 40 is in the "0", *i.e.*, cutoff, position, then the volume of PGM1 is -100 dB, *i.e.*, 100 dB down, and for all practical purposes PGM1 has zero volume and is thus inaudible in the MASTER EFFECTS signal. Conversely, if the control 40 is in the "10", *i.e.*, full, position, then the volume
25 of PGM1 is 0 dB, which is full volume in this version of the control 40.

Referring to Figures 2 and 3, the mixer 16 may include reversal controls (not shown in Figure 2) — one for each of the controls 40 and 42 — for reversing the cutoff and full positions of the controls 40 and 42, respectively. Such controls are known as "hamsters" in turntablist jargon, and are included so that the turntablist can
30 attain the most comfortable hand positions while performing his piece. In operation, if the reversal control is in one position, then the "0" position of the control 40 is the cutoff position and the "10" position is the full position as discussed above.

Conversely, if the reversal control is in another position, then the “0” position is the full position and the “10” position is the cutoff position.

Referring again to Figures 2 and 3, the mixer 16 may include contour controls (not shown in Figure 2) — one for each of the controls 40 and 42 — for adjusting the shape of the curve 43. Contour controls typically allow the turntablist more flexibility in playing his musical piece. In operation, a change in the shape of the curve 43 changes the distance that the turntablist must move the control 40 to get a given change in the volume of PGM1. For example, the turntablist may want to transition PGM1 from cutoff to full volume by moving the control 40 only a fraction of the distance between the “0” and “10” positions instead of the entire distance as the illustrated shape of the curve 43 requires. Therefore, the turntablist sets the contour control such that the curve 43 has a shape that is steeper in the cutoff region than illustrated in Figure 3.

Referring again to Figure 2, the mixer 16 also includes a crossfader control 44 for adjusting the ratio of the volume of PGM1 to the volume of PGM2 — the volumes of PGM1 and PGM2 also being set by the fader controls 40 and 42, respectively — in the MASTER signal. Like the fader controls 40 and 42, the crossfader control 44 is typically a sliding control that the turntablist uses to vary this volume ratio for musical effect while he is playing his piece.

Figure 4 is a plot of curves 45 and 46, which respectively show the attenuation in decibels for PGM1 and PGM2 versus the control position for a known embodiment of the crossfader control 44. In operation, referring to both Figures 2 and 4, if the control 44 is all the way to the left in the PGM1 “10”/PGM2 “0” position, *i.e.*, full position for PGM1 and cutoff position for PGM2, then the volume of PGM1 is full and the volume of PGM2 is 100 dB down, and for all practical purposes PGM1 is the only audible component of the MASTER EFFECTS signal. Conversely, if the control 44 is all the way to the right in the PGM1 “0”/PGM2 “10” position, *i.e.*, cutoff position for PGM1 and full position for PGM2, then the volume of PGM1 is 100 dB down and the volume of PGM2 is full, and for all practical purposes PGM2 is the only audible component of the MASTER EFFECTS signal.

The mixer 16 may also include a reversal control, *i.e.*, “hamster” (not shown in Figure 2), for reversing the cutoff and full positions of the control 44 with respect to

PGM1 and PGM2. In operation, if the reversal control is in one position, then the leftmost position of the control 44 is the PGM1-full/PGM2-cutoff position and the rightmost position is the PGM1-cutoff/PGM2-full position as discussed above. Conversely, if the reversal control is in another position, then the leftmost position of the control 44 is the PGM1-cutoff/PGM2-full position and the rightmost position is the PGM1-full/PGM2-cutoff position.

Still referring to Figures 2 and 4, the mixer 16 may also have a contour control (not shown in Figure 2) for adjusting the shapes of the curves 45 and 46 in a manner similar to that discussed above for adjusting the shape of the curve 43 of Figure 3.

Furthermore, the illustrated shapes of the curves 45 and 46 may represent a constant-power crossfader contour. In other words, regardless of the position of the crossfader control 44, the sum of the powers, and thus the volumes, of PGM1 and PGM2 in the MASTER EFFECTS signal equals a constant level.

Unfortunately, movement of the fader controls 40 and 42 often adds audible levels of noise called "travel" noise, to PGM1 and PGM2, respectively. Additionally, because they are in the respective PGM1 and PGM2 signal paths, the fader controls 40 and 42 may allow audible levels of PGM1 and PGM2 to "bleed into" the MASTER EFFECTS signal even if the controls 40 and 42, respectively, are in their full-cut positions.

One way to reduce both travel noise and signal bleed through is to use high quality, low-noise controls, such as low-noise potentiometers, for the controls 40 and 42. But these low-noise potentiometers are relatively expensive, and, like their cheaper counterparts, soon wear down to a point where they generate unacceptable travel noise or allow unacceptable signal bleed through, and thus must be replaced.

Another way to reduce the travel noise is to remove the input-fader controls 40 and 42 from the PGM1 and PGM2 signal paths, respectively. Thus the output signals from the controls 40 and 42 can be filtered and then used to control the gain of an audio amplifier. Unfortunately, such designs are frequently expensive, complex, and lack the consistent performance required by turntablists. For example, the filter may cause the controls 40 and 42 to exhibit inappropriate volume-increase and volume-decrease rates — often called "attack" and "decay" rates, respectively — which may compromise the ability of the filter to remove travel noise without adversely altering the performance of the turntablist. In addition, such designs

frequently require a separate gain-controlled amplifier for each fader control 40 and 42, thus making the input-fader circuit too complex and expensive for compact performance mixers.

5 The crossfader control 44 may also add audible levels of travel noise and signal "bleed" to PGM1 and PGM2. Noise-reduction techniques similar to those discussed above for the controls 40 and 42 may be used to reduce the travel noise generated by the crossfader control 44. Unfortunately, these techniques often exhibit the same shortcomings as the above-described techniques.

10 Furthermore, many crossfader contour controls lack a constant-power setting. And like the input-fader circuits, the crossfader circuit may allow audible levels of PGM1 and PGM2 to bleed into the MASTER EFFECTS signal even if the control 44 is in its respective PGM1-full-cut or PGM2-full-cut position.

15 Furthermore, the input-fader circuits are often highly sensitive to component tolerances such that the same absolute positions of the respective controls 40 and 42 may provide different attenuations for different mixers 16. For example, suppose that controls 40 of two mixers 16 are in their respective "6" positions. Because of the high sensitivities of the respective input-fader circuits, however, the first mixer may attenuate PGM1 by 20 dB and the second mixer may attenuate PGM1 by 18 dB. Often, the turntablist practices on one mixer 16 and performs on another mixer 16, and is, therefore, used to the position-attenuation characteristics for the controls 40 and 42 of the practice mixer. Consequently, if the position-attenuation characteristics of the performance mixer are different than those of the practice mixer, then the performed piece will not sound as the turntablist intended. Thus, differences in the input-fader position-attenuation characteristics between the practice and performance mixers can ruin the turntablists performance!

25 Like the input-fader circuits, the crossfader circuit is often highly sensitive to component tolerances, and thus may cause the crossfader control 44 to exhibit different position-attenuation characteristics from mixer to mixer. Moreover, because the design of the crossfader circuit is often complex, the crossfader circuit often requires a relatively large number of components and thus contributes significantly to the cost, size, and power consumption of the mixer 16.

30 Furthermore, referring to Figure 1, if the turntablist wants to use the effects box 18 to add audio effects to either PGM1 or PGM2, then he must disconnect the

box 18 from MASTER and reconnect it between the respective turntable 12 or 14 and the mixer 16. This makes it virtually impossible for the turntablist to add effects to more than one of the PGM1, PGM2, and MASTER signals while he plays his piece. One solution is to use three effects boxes 18: one for PGM1, one for PGM2, and one for MASTER. But unfortunately, because the effects box 18 is a relatively expensive item, most turntablists can afford to have only one.

Moreover, to allow independent gain control of the bass and treble frequency components, the mixer 16 often includes bass-band, mid-band, and treble-band filters, which are collectively called a tone-control circuit or simply a tone control.

Unfortunately, the frequency cutoff slopes of many tone-control circuits are not steep enough to allow for such independent gain control. One solution is to use a 4th-order tone-control circuit. But the filters used in a 4th-order tone-control circuit often have relatively large numbers of components, and thus often increase the cost, size, and power consumption of the mixer 16.

SUMMARY OF THE INVENTION

In one aspect of the invention, an audio-signal circuit includes a 4th-order low-pass filter circuit having a first phase response, the filter circuit receiving and filtering an audio signal and generating a first output signal therefrom, a 4th-order band-pass filter having a second phase response that is substantially equal to the first phase response, the band-pass filter circuit receiving and filtering the audio signal to generate a second output signal, a 4th-order high-pass filter circuit having a third phase response substantially equal to the first and second phase responses, the high-pass filter circuit receiving and filtering the audio signal to generate a third output signal, and a combining circuit that combines the first, second and third output signals into a combined signal. In another embodiment, the audio signal circuit is implemented with 2nd-order filters instead of 4th-order filters.

Such a circuit provides useful levels of isolation between the frequency bands of an audio signal with significantly fewer components than prior circuits. Thus, such a circuit costs significantly less to manufacture than prior circuits, and also occupies a reduced circuit board area, which contributes to a significantly lower cost of a device such as an audio mixer that incorporates the filter circuit.

BRIEF DESCRIPTION OF THE DRAWINGS

Figure 1 is a block diagram of a turntablist's sound system according to the prior art.

Figure 2 shows the control panel for the audio mixer of Figure 1.

5 Figure 3 is a plot of signal attenuation versus control position for the input-fader controls of Figure 2.

Figure 4 is a plot of signal attenuation versus control position for the crossfader control of Figure 2.

10 Figure 5A shows the control panel for an embodiment of an audio mixer according to the invention.

Figure 5B shows the power and signal jacks on one side of the mixer of Figure 5A.

Figure 5C shows the controls on another side of the mixer of Figure 5A.

15 Figure 5D is a block diagram of a sound system that incorporates the mixer of Figures 5A-C.

Figure 6 is a schematic block diagram of the circuitry for an embodiment of the mixer of Figure 5A - C.

Figures 7A-7C are a schematic diagram of an embodiment of the circuitry of Figure 6.

20 Figure 8 is a schematic diagram of an embodiment of the input-fader circuit of Figure 6.

Figure 9 is a plot of signal attenuation versus control position for the different contour settings of the input-fader circuit of Figure 8.

25 Figure 10 is a block diagram of an embodiment of the crossfader circuit of Figure 6.

Figure 11A is a plot of signal attenuation versus control position for a first setting of the contour control of the crossfader circuit of Figure 10.

Figure 11B is a plot of signal attenuation versus control position for a second setting of the contour control of the crossfader circuit of Figure 10.

30 Figure 11C is a plot of signal attenuation versus control position for a third setting of the contour control of the crossfader circuit of Figure 10.

Figure 12 is a schematic block diagram of an embodiment of the crossfader circuit of Figure 10.

Figure 13 is a schematic diagram of an embodiment of the crossfader circuit of Figure 12.

Figure 14 is a block diagram of an embodiment of the gain core and fader-control circuit of Figure 6.

5 Figure 15 is a schematic diagram of an embodiment of the gain core of Figure 14.

Figure 16 is a block diagram of an embodiment of one of the tone-control circuits of Figure 6.

10 Figure 17 is a Bode plot of the gain and phase responses for an embodiment of the tone-control circuit of Figure 16 showing respective ranges of the bass-band and treble-band gains.

Figure 18 is a Bode plot of the gain and phase for the tone-control circuit of Figure 16 showing a range for the mid-band gain.

15 Figure 19 is a schematic diagram of an embodiment of the tone-control circuit of Figure 16.

Figure 20 is a block diagram of another embodiment of the tone-control circuit of Figure 16.

Figure 21 is a block diagram of another embodiment of the tone-control circuits of Figure 6.

20 Figure 22 is a Bode plot of the gain and phase responses for an embodiment of the tone-control circuit of Figure 21 showing respective ranges for the bass-band and treble-band gains.

Figure 23 is a Bode plot of the gain and phase responses for an embodiment of the tone-control circuit of Figure 21 showing a range for the mid-band gain.

25 Figure 24 is a schematic diagram of an embodiment of the tone-control circuit of Figure 21.

Figure 25 is a block diagram of an embodiment of the effects-loop multiplexer of Figure 6.

30 Figures 26A-26B are a schematic diagram of an embodiment of the effects-loop multiplexer of Figure 25.

DETAILED DESCRIPTION OF THE INVENTION

Figures 5A – C are respective views of an audio mixer according to an embodiment of the invention, and Figure 5D is a block diagram of a sound system that incorporates the audio mixer of Figures 5A - C.

5 Figure 5A is a top view of a mixer 50 according to an embodiment of the invention. For example, the mixer 50 may be a TTM 54 Performance Mixer manufactured by RANE Corporation of Mukilteo, Washington. The mixer 50 includes a control panel 52, which includes an all-band gain control 54 and bass-band and treble-band gain controls 56 and 58 for the PGM1 signal, and which includes an all-
10 band gain control 60 and bass-band and treble-band gain controls 62 and 64 for the PGM2 signal. The all-band gain controls 54 and 60 function like the controls 28 and 30, respectively, of Figure 2. The bass-band and treble-band gain controls 56, 58, 62, and 64 function like the controls 32, 36, 34, and 38, respectively, of Figure 2, but the tone-control circuits of the mixer 50 (not shown in Figure 5A) are significantly
15 improved over the prior-art tone-control circuits as discussed below in conjunction with Figures 16 - 24.

The mixer 50 also includes respective PGM1 and PGM2 input-fader controls 66 and 68, respective PGM1 and PGM2 input-fader contour controls 70 and 72, and respective PGM1 and PGM2 input-fader reversal controls, *i.e.*, “hamsters”, 74 and
20 76. The fader controls 66 and 68 function like the controls 40 and 42 of Figure 2 and the contour and reversal controls function like the contour and reversal controls described in the Background of the Invention. But the input-fader circuits of the mixer 50 — which incorporate the input-fader, contour, and reversal controls 66, 68, 70, 72, 74 and 76 and which are discussed below in conjunction with Figures 8 - 9 —
25 are significantly improved over the prior-art input-fader circuits.

Additionally, the mixer 50 includes a crossfader control 78, crossfader contour control 80 (Figure 5C), and crossfader reversal control 82 (Figure 5C), which respectively function like the crossfader control 44 and the crossfader contour and reversal controls discussed in the Background. But the crossfader circuit of the
30 mixer 50 — which incorporates the crossfader, contour, and reversal controls 78, 80, and 82 and which is discussed below in conjunction with Figures 10 - 13 — is significantly improved over the prior-art crossfader circuits.

Furthermore, the mixer 50 includes assignable-effects controls 84 and 86, which, depending upon their respective settings, route one of the PGM1, PGM2, or MASTER signals through the effects box 18 (Figure 5D).

5 The mixer 50 may also include conventional microphone controls 87, conventional headphone controls 88, a conventional master/cue control 89, conventional PGM1 and PGM2 balance controls 90 and 91, conventional PGM1 and PGM2 phone/line switches 92 and 93, and a conventional LED volume display 94.

Thus, unlike prior-art mixers like the mixer 16 of Figure 2, the mixer 50 includes input-fader contour and input-fader reversal controls and crossfader contour and crossfader reversal controls. The mixer 50 also allows a turntablist to route PGM1, PGM2, or MASTER through the effects box 18 (Figure 5D) without having to physically disconnect and reconnect the box 18. Additionally, the mixer 50 provides many other improvements as described below.

Figure 5B is a side view that shows the signal and power jacks of the mixer 50. Because it can mix and generate both monaural and stereo audio signals, the mixer 50 has two connectors, a left (L) connector and a right (R) connector, for each potential source (line or phono) of the PGM1 and PGM2 signals and each potential termination (balanced or unbalanced) of the MASTER signal. For monaural operation, either the L connectors or the R connectors may be used. The phono connectors allow the mixer 50 to receive PGM1 and PGM2 from turntables like the turntables 12 and 14 (Figure 5D), and the line connectors allow the mixer 50 to receive PGM1 and PGM2 from other sources such as a radio receiver, compact disc (CD) player, or tape player. Furthermore, unlike prior-art mixers, the mixer 50 includes both send and return connectors for the effects box 18 (Figure 5D) so that the controls 84 and 86 can route one of the PGM1, PGM2, and MASTER signals to the effects box 18 via the send connectors and can receive the signal, which has added audio effects, from the effects box 18 via the return connectors. The mixer 50 also includes a conventional microphone input connector and microphone-effects send and return connectors, which allow the mixer 50 to send the microphone signal to a microphone effects box (not shown) and to receive therefrom the microphone signal having added audio effects.

Figure 5C is another side view of the mixer 50 that shows the crossfader contour and reversal controls 80 and 82, which are discussed above in conjunction

with Figure 5A, a conventional all-band volume-level control for the MASTER signal, and a conventional headphone connector.

Figure 5D is a block diagram of a sound system 95, which incorporates the mixer 50 of Figures 5A - 5C and which has like numerals for like elements with respect to Figures 1 and 5A. The sound system 95 is similar to the sound system 10 of Figure 1 except that the mixer 50 replaces the prior-art mixer 16 and the effects box 18 has both its input and output terminals coupled to the mixer 50 as discussed above in conjunction with Figure 5B. As discussed below, the mixer 50 incorporates improvements that make it superior to the prior-art mixer 16, and thus make the sound system 95 superior to the sound system 10.

Figure 6 is a block diagram of the circuitry for an embodiment of the mixer 50 of Figures 5A - D, where like numerals are used for like elements with respect to Figures 5A - D and where circuits not pertinent to the invention are omitted for clarity.

The mixer 50 includes conventional PGM1 and PGM2 preamplifier and balance circuits 96a and 96b, which respectively include the gain and balance controls 54 and 90 and 60 and 91 and which respectively adjust the gains and balances of PGM1 and PGM2 in response thereto. Tone-control circuits 97a and 97b are respectively coupled to the circuits 96a and 96b, respectively include the bass and treble controls 56 and 58 and 62 and 64, and adjust the bass-band and treble-band gains of PGM1 and PGM2, respectively, based on the settings of these controls. In one embodiment, the circuits 97a and 97b also include respective controls for adjusting the mid-band gains of PGM1 and PGM2 as discussed above in conjunction with Figures 16 - 24. In another embodiment, the circuits 97a and 97b provide steep frequency-cutoff slopes, and thus allow independent control of the bass-, mid-, and treble-band gains, with fewer components than prior-art tone-control circuits.

The mixer 50 also includes an effects-path multiplexer 98, which includes the assignable-effects controls 84 and 86. The multiplexer 98 receives PGM1 and PGM2 from the tone-control circuits 97a and 97b, respectively, and receives the MASTER signal from a gain core 99. Depending upon the settings of the controls 84 and 86, the multiplexer 98 couples one or none of the PGM1, PGM2, or MASTER signals through an effects path that includes the effects box 18 (Figure 5D). If the

multiplexer 98 does couple one of these signals through the effects path, it receives the return signal — which has audio effects added — from the effects box 18, and then provides the return signal to the respective one of the PGM1, PGM2, and MASTER output terminals. Conversely, the multiplexer 98 merely passes through, from input to output, the signals that it does not route through the effects path.

The gain core 99 amplifies PGM1 and PGM2 from the multiplexer 98 in response to one or more gain-control signals that are generated by a fader control circuit 102, which includes an input-fader circuit 104 and a crossfader circuit 106. The input-fader circuit 104 includes the input-fader, contour, and reversal controls 66, 70, and 74 for adjusting PGM1 and includes the input-fader, contour, and reversal controls 68, 72, and 76 for adjusting PGM2. Likewise, the crossfader circuit includes the crossfader, contour, and reversal controls 78, 80, and 82. After amplifying PGM1 and PGM2, the gain core 99 mixes these signals together to generate the MASTER signal, which the gain core 99 provides to an input of the effects-path multiplexer 98 as discussed above.

An output amplifier 108 amplifies the MASTER signal from the multiplexer 98 and provides the amplified MASTER signal to the MASTER connector(s) of Figure 5B.

In operation, before playing his piece, a turntablist adjusts the controls, *e.g.*, 54 and 90 and 60 and 91, of the circuits 96a and 96b to give the desired amounts of gain and balance to PGM1 and PGM2, respectively. He also adjusts the controls, *e.g.*, 56 and 58 and 62 and 64, of the tone-control circuits 97a and 97b to provide the desired gain or cut in the bass, mid, and treble-bands of PGM1 and PGM2, and if he desires audio effects, he adjusts the controls, *e.g.*, 84 and 86, of the multiplexer 98 to route one of the signals PGM1, PGM2, and MASTER through the effects path. Additionally, the turntablist adjusts the input-fader and crossfader contour controls 70, 72, and 80 and reversal controls 74, 76, and 82 to the desired settings. Although the turntablist typically adjusts the above controls before performing his piece, he may adjust them while playing his piece as well. Then, while playing his piece, the turntablist manipulates the input-fader controls 66 and 68 and the crossfader control 78. As they move, the controls 66, 68, and 78 vary the gains that the core 99 imparts to PGM1 and PGM2 before it mixes them together. These gain variations cause the changes in the volumes and mixing ratio of PGM1 and PGM2 that give the

desired musical effects. The output amplifier 108 amplifies the MASTER signal and provides it to the house amplifier 20 (Figure 5D) so that the audience can hear the turntablist's musical piece.

Figures 7A-7C are a schematic diagram of an embodiment of the mixer circuitry of Figure 6. Unlike Figure 6, Figure 7 shows the L and R components of PGM1, PGM2, and MASTER. Furthermore, Figure 7 shows the portions 98a and 98b of the effects-path multiplexer 98 for processing the L and R components, respectively, of PGM1, PGM2, and MASTER.

INPUT-FADER CIRCUIT

Figure 8 is a schematic diagram of a portion of the input-fader circuit 104 of Figure 6 according to an embodiment of the invention. For clarity, only the portion that controls the volume of PGM1 is shown, the portion that controls the volume of PGM2 being similar.

The circuit 104 includes the input-fader control 66, the contour control 70, and the reversal control 74, which in this embodiment are a potentiometer, a three-position switch, and a two-position switch, respectively.

The reversal control 74 reverses the full-volume and cut-volume positions of the control 66 by reversing the voltage polarity across it. Specifically, the unmovable terminals of the control 66 are respectively coupled to terminals 110 and 112 of the reversal control 74. In the illustrated position, the control 74 couples the terminals 110 and 112 to a voltage V and ground, respectively, and in its other position, the control 74 couples the terminals 110 and 112 to ground and V respectively.

The control 66 includes a wiper arm 114, which is what moves when the turntablist moves the control 66. The arm 114 divides the control 66 into two resistors having respective values that depend on the position of the arm 114. Thus, based on the well-known voltage-divider principle, the voltage at the arm 114 depends on a ratio of the values of these two resistors. For example, if the arm 114 is in the middle position, the two resistors are equal and the voltage at the arm 114 is $V/2$. The control 66 provides this voltage, which is called an input-fader gain-control voltage, to the gain core 99 (Figure 6) to control the gain of the PGM1 amplifier therein. Because this gain-control voltage, and thus the gain of the PGM1 amplifier, depends more on the ratio of the resistor values than on the actual resistor values,

the control 66 is called a ratiometric control, which significantly reduces the component-tolerance sensitivity of the circuit 104. Thus, the respective position-attenuation characteristics of the controls 66 are significantly more repeatable from mixer to mixer than the position-attenuation characteristics of the controls 40 and 42 of Figure 2.

The contour control 70 is part of a contour circuit 116, which adds a load to the wiper arm 114 to vary the shape of the position-versus-attenuation curve (Figure 9) of the control 66. Specifically, the arm 114 is coupled to terminals 117 and 118 of the control 70, which depending upon its setting, couples the arm 114 to a respective one of different-sized contour resistors 120, 122, and 124. As discussed further below in conjunction with Figure 9, each contour resistor presents a different load to the arm 114 and thus causes the position-versus-attenuation curve to have a different shape.

The circuit 104 also includes resistors 126 and 128 and a light-emitting diode (LED) 130. The LED 130 turns on if the reversal switch 74 is in the reverse position (the position opposite that shown in Figure 8). The resistor 128 limits the current through the LED 130. Because the source (not shown) that generates V may have a relatively high output impedance, the resistor 126 is included to balance the load "seen" by the source so that V remains relatively constant regardless of the position of the switch 74.

In operation while performing his piece, the turntablist moves the control 66 such that the gain-control voltage has a value between V and ground. In one embodiment, full gain, and thus full volume, correspond to the gain-control voltage equaling ground, and minimum gain, and thus volume cutoff, correspond to the gain-control voltage equaling V . Before or while performing his piece, the turntablist may switch the reversal control 74 to reverse the full and cut positions of the control 66, and may switch the contour control 70 to change the slope of the attenuation-versus-position curve of the control 66.

In one embodiment of the input-fader circuit 104, the cutoff level of the gain-control signal is sufficient to prevent PGM1 from bleeding into the MASTER signal. In another embodiment, $V = -3.2$ Volts. In yet another embodiment, the resistors 120, 122, 124, 126, and 128 have the following respective values: 7.5 k Ω , 37.4k Ω , 90.9k Ω , 1k Ω and 243 Ω , and the control 66 has a value of 200k Ω . In still another

embodiment, the control 66 is removable to allow field replacement because it may wear out several times during the lifetime of the mixer 50. In yet another embodiment that is discussed below in conjunction with Figure 14, an optional low-pass filter 131 is included between the arm 114 and the gain core 99 (Figure 6) to reduce travel noise caused by the movement of the control 66. The filter 131 typically has a corner frequency in the range of approximately 10 – 50 Hz. A corner frequency of approximately 45 Hz has been found to provide good noise reduction without noticeably slowing the response time of the control 66. In still another embodiment, the control 66 is an optical control that generates an optical digital signal proportional to its position, and the circuit 104 includes circuitry for processing this digital signal and generating the gain-control signal therefrom. In yet another embodiment, the contour circuit 116 provides more or fewer than three discrete contour settings. In still another embodiment, the switch 70 and the resistors 120, 122, and 124 of the contour circuit 116 are replaced with a potentiometer such that the circuit 116 provides a continuous range of contour settings.

Therefore, in addition to the previously mentioned advantages, unlike the designs of many prior-art fader circuits, the design of the circuit 104 allows it to have both a reversal control and a contour control. Furthermore, in the cutoff position, the circuit 104 can reduce the gain of the PGM1 amplifier in the gain core 99 (Figure 6) enough to prevent bleed through of PGM1 into the MASTER signal. Additionally, the circuit 104 reduces or eliminates cross-talk between PGM1 and PGM2.

Figure 9 is a plot of three curves 132, 134, and 136, which show the attenuation of PGM1 caused by the gain-control signal versus the position of the control 66 for the three settings of the contour control 70 of Figure 8. These curves represent the embodiment of the contour control circuit 116 in which the resistors 120, 122, and 124 have the values given above. Because of the design of the circuit 116, these curves do not have constant slopes, *i.e.*, are not straight lines. The curve 132 corresponds to the control 70 coupling the smallest resistor, here the 7.5k Ω resistor 120, to the wiper 114. The curve 132 has the most gradual slope until the control 66 is almost at the cutoff position, at which point the curve 132 has a very steep slope that is suitable for switching between cutoff and nearly full volume with a relatively small movement of the control 66. The curve 134 corresponds to the control 70 coupling the middle-valued resistor, here the 37.4k Ω resistor 122, to the

wiper 114. The curve 134 generally has a steeper slope than the curve 132 until the control 66 is almost at cutoff, at which point the curve 134 has a more gradual slope than the curve 132. The curve 136 has a nearly constant slope, and corresponds to the control 70 coupling the largest resistor, here the 90.9k Ω resistor 124, to the wiper 114. By changing the values of the resistors 120, 122, and 124, one can change the shapes of the curves 132, 134, and 136, respectively. Furthermore, in another embodiment, the circuit 116 is designed to provide the curves 132, 134, and 136 having different shapes such as straight lines or nearly straight lines having different slopes.

CROSSFADER CIRCUIT

Figure 10 is a block diagram of an embodiment of the crossfader circuit 106 of Figure 6. The circuit 106 includes a crossfader contour circuit 138, which includes the contour control 80 and which generates a contour signal in response to the setting of the control 80. A bias circuit 140 generates a bias signal from the sum of a reference signal and a contour signal. A crossfader-control-signal generator 142 includes the crossfader control 78 and generates first and second gain-control signals. The respective values of the first and second gain-control signals depend on the position of the control 78 and the values of the contour and bias signals. A reversal circuit 144, which includes the reversal control 82, receives the first and second gain-control signals. Depending on the setting of the reversal control 82, the circuit 144 provides the first and second gain-control signals to control the respective gains of the PGM1 and PGM2 amplifiers of the gain core 99 (Figure 6) or vice versa. As discussed above in conjunction with Figure 8 and further below in conjunction with Figure 14, the crossfader circuit 106 may also include low-pass filters 146a and 146b to limit the frequency response of the control 78 so as to reduce audible travel noise when the turntablist moves the control 78 without reducing the response time of the control 78 below acceptable levels. In one embodiment, the filters 146a and 146b have respective corner frequencies in the range of approximately 10 – 50 Hz, for example approximately 45 Hz.

In operation, the turntablist adjusts the contour control 80 as desired. The contour signal from the contour circuit 138 sets the slope of the attenuation-versus-position curves (Figures 11A – 11C) of the first and second gain-control signals. In

one embodiment, the bias signal has a value such that at the respective full-volume positions of the control 78, the circuit 142 generates the first and second gain-control signals such that the PGM1 and PGM2 amplifiers of the gain core 99 (Figure 6) have a maximum gain of one. The turntablist also adjusts the reversal control 82 to set the PGM1 and PGM2 full/cut positions of the control 78, and moves the control 78 while playing his piece to vary the values of the first and second gain-control signals. Thus, by varying the values of these gain-control signals, the turntablist varies the volume ratio of PGM1 and PGM2 in the MASTER signal.

Figure 11A is a plot of two curves that respectively show PGM1 and PGM2 attenuation versus control 78 position for one setting of the contour control 80 of Figure 10. That is, one curve shows the attenuation of PGM1 caused by the corresponding gain-control signal, and the other shows the attenuation of PGM2 caused by the other gain-control signal. At this contour-control setting, the sum of the powers of PGM1 and PGM2 is nearly or exactly constant as discussed above in conjunction with Figure 4. Thus, the volume of MASTER is nearly or exactly constant regardless of the position of the crossfader control 78. In one embodiment, the maximum deviation from constant power is ± 0.5 dB. Furthermore, the achievement of constant power is based on an assumption that PGM1 and PGM2 include equal or nearly equal root-mean-square (RMS) levels of incoherent signals. Thus, if PGM1 and PGM2 migrate from this condition, the maximum deviation from constant power may increase.

Figure 11B is a plot of two curves that respectively show PGM1 and PGM2 attenuation versus control 78 position for another setting of the contour control 80 of Figure 10. At this contour setting, the slopes of the curves are relatively steep such that a relatively small movement of the crossfader control 78 — approximately 20% of full range — near its full/cut positions transitions the respective PGM1 and PGM2 signals between cutoff and full volume. At and around the middle position of the control 78, the mixing ratio of PGM1 to PGM2 equals 1:1.

Figure 11C is a plot of two curves that respectively show PGM1 and PGM2 attenuation versus control 78 position for yet another setting of the contour control 80 of Figure 10. At this contour setting, the slope of the curves are even steeper than slopes of the curves in Figure 11B, so that an even smaller movement of the

crossfader control 78 — approximately 3% of full range, which is approximately 2 millimeters in one embodiment — near its full/cut positions transitions the respective PGM1 and PGM2 signals between cutoff and full volume.

Thus, the crossfader circuit 106 of Figure 10 includes both a contour circuit 138 and a reversal circuit 144. Additionally, the contour circuit 138 allows the attenuation-versus-position curves to have contours ranging from constant power (Figure 11A) to fast cut-in/cut-out (Figure 11C). Furthermore, the circuit 106 generates the first and second gain-control signals such that at the full-cut positions of the control 78, the gain-control signals prevent bleed through of PGM1 or PGM2, respectively, into MASTER.

Figure 12 is a schematic block diagram of an embodiment of the crossfader circuit 106 of Figure 10.

In this embodiment, the contour control 80 is a ratiometric control that includes a potentiometer having its two stationary terminals coupled between voltages V1 and V2. The control 80 generates a contour voltage V_{contour} on its wiper arm 147, which is coupled to the input terminal of an amplifier 148. The bias circuit 140 includes a signal combiner 150, which combines V_{contour} from the circuit 138 with a reference voltage V_{ref} . The circuit 140 also includes an amplifier 152, which generates a bias signal V_{bias} from the combiner 150 output signal. In this embodiment, the combiner 150 is a summer circuit.

The crossfader control 78 is also a ratiometric control that includes a potentiometer having a wiper arm 154 coupled to receive V_{bias} from the bias circuit 140. (It is the wiper arm 154 that moves when the turntablist moves the control 78.) The control 78 generates respective portions of V_{bias} at its stationary terminals, the values of these respective portions depending on the position of the wiper arm 154. The larger the value of V_{bias} , the greater the change in the respective portions of V_{bias} at the stationary terminals of the control 78, and thus the greater the changes in the gain-control voltages $V_{\text{gain-control1}}$ and $V_{\text{gain-control2}}$. The crossfader-control-signal generator 142 includes signal combiners 156a and 156b, which are summer circuits in this embodiment and which combine V_{contour} with the respective portions of V_{bias} generated by the control 78 at its stationary terminals. For example, suppose the arm 154 is in the upper full/cut position such that it is directly coupled to the combiner 156a. Thus, the full value of V_{bias} is coupled to the

amplifier 186, which acts as both the combiner 150 and amplifier 152 of Figure 12. In one embodiment, the values of these resistors respectively equal 26.7kΩ, 3.16kΩ, 200kΩ, and 200kΩ, and Vref is −15V. The crossfader control circuit 142 includes a potentiometer for the crossfader control 78, input resistors 188a, 188b, 190a, and 190b, feedback resistors 192a and 192b, feedback diodes 194a, 194b, 196a, and 196b, and amplifiers 198a and 198b, which act as both the combiner circuits 156a and 156b and the amplifiers 158a and 158b, respectively, of Figure 12. In one embodiment, the values of all these resistors equal 6.34kΩ, and the value of the crossfader potentiometer is 200kΩ. In such an embodiment, the amplifiers 198a and 198b each have a gain of -1, and thus the maximum value of Vgain-control1 and Vgain-control2 is -[Vbias + Vcontour]. Furthermore, the crossfader control 78 may be field replaceable.

In operation, because the amplifier 148 is connected in an inverting configuration and V1 and V2 are negative, the contour circuit 138 generates a positive voltage for Vcontour, the exact value of Vcontour depending on the setting of the control 80. In one embodiment where the amplifier 148 has unity gain, Vcontour is within a range of 94 millivolts(mV) to 3.67V.

The bias circuit 140 generates Vbias according to the following equation:

$$(1) \quad V_{bias} = \left[-V_{contour} \frac{R_{184}}{R_{182}} + V_{ref} \frac{R_{180}}{R_{178} + R_{180}} \left(1 + \frac{R_{184}}{R_{182}} \right) \right]$$

Because Vcontour is subtracted from Vbias and added to Vgain-control1, it is possible for the value of Vcontour to affect the response of the crossfader control 78 while the crossfader circuit 106 maintains a constant, maximum attenuation level. In addition, limiting the value of Vgain-control1 to non-negative values prevents Vcontour from affecting the maximum gain. Thus, Vcontour affects only the response of the crossfader control 78 and not the maximum gain or attenuation provided by the circuit 106.

The crossfader control circuit 142 generates Vgain-control1 as a combination of Vcontour and the portion of Vbias provided by the crossfader control 78. Specifically, because Vcontour is positive, the amplifier 148 sources a current into

the input resistor 188a and thus tends to lower the output voltage of the amplifier 198a. Conversely, because V_{bias} is negative, the portion of V_{bias} generated by the control 78 is also negative. Thus, the control 78 sources a current into the input resistor 190a and thus tends to raise the output voltage of the amplifier 198a.

5 In the embodiment where the resistors 188a, 190a, and 192a equal the same value, if the absolute value of $V_{contour}$ is greater than the absolute value of the portion of V_{bias} provided by the control 78, then $V_{gain-control1}$ equals and is limited to a 0 V minimum. In one embodiment, $V_{gain-control1} = 0$ V causes the PGM1 amplifier in the gain core 99 (Figure 6) to have a maximum gain of 1, which
10 corresponds to the 0 dB (maximum gain) level of the curves in Figures 11A – 11C. More specifically, if the absolute value of $V_{contour}$ is greater than the absolute value of the portion of V_{bias} , then the current through the resistor 188a is greater than the current through the resistor 190a. This causes a difference current to flow through the diode 194a to the output of the amplifier 198a, thus causing the output voltage of
15 the amplifier 198a to be negative. But this negative output voltage reverse biases the diode 196a, which thus prevents the output of the amplifier 198a from sinking a current from the feedback resistor 192a. Therefore, because no current flows through the resistor 192a, $V_{gain-control1}$ equals and cannot go lower than 0 V, which is the voltage at the inverting terminal of the amplifier 198a.

20 Conversely, if the absolute value of $V_{contour}$ is less than the absolute value of the portion of V_{bias} provided by the control 78, then $V_{gain-control1}$ equals a positive voltage that depends on the difference between $V_{contour}$ and the portion of V_{bias} . In one embodiment, the more positive $V_{gain-control1}$ is, the lower the gain — and thus the higher the attenuation provided by — the PGM1 amplifier in the gain
25 core 99 (Figure 12). More specifically, if the absolute value of $V_{contour}$ is less than the absolute value of the portion of V_{bias} , then the current through the resistor 188a is less than the current through the resistor 190a. This causes a difference current to flow through the feedback resistor 192a and the forward-biased diode 196a, thus causing the output voltage of the amplifier 198a to be positive. Therefore, because a
30 feedback current flows through the resistor 192a, $V_{gain-control1}$ equals a positive value that is proportional to this feedback current. Furthermore, based on this analysis, the cut-off position of the control 78 with respect to $V_{gain-control1}$ is the wiper 154 being all the way toward the input resistor 190a such that the control 78

sinks a maximum current from the resistor 190a. Consequently, the full-volume position with respect to Vgain-control1 is the wiper 154 being all the way toward the resistor 190b.

From the above analysis, it is clear that low values of Vcontour cause the attenuation-versus-position curve for Vgain-control1 to have a relatively gradual slope, and high values of Vcontour cause this curve to have a relatively steep slope. Specifically, for relatively low values of Vcontour, a relatively small movement of the arm 154 from the Vgain-control1 full-volume position causes the current through the resistor 190a to become greater than the current through the resistor 188a. Thus, the lower the value of Vcontour, the greater the position range over which the control 78 can generate a positive, *i.e.*, attenuation, voltage for Vgain-control1. Therefore, a low value for Vcontour causes the circuit 142 to provide a attenuation-versus-position curve having a relatively gradual slope like the PGM1 curve of Figure 11A. Conversely, for relatively large values of Vcontour, a relatively large movement of the arm 154 from the Vgain-control1 full-volume position is needed before the current through the resistor 190a becomes greater than the current flowing through the resistor 188a. Thus, the greater the value of Vcontour, the smaller the position range over which the control 78 can generate a positive, *i.e.*, attenuation, voltage for Vgain-control1. Therefore, a large value for Vcontour causes the circuit 142 to provide an attenuation-versus-position curve having a relatively steep slope like the PGM1 curves of Figures 11B and 11C.

Furthermore, as discussed above, in one embodiment, the maximum attenuation that Vgain-control1 causes in PGM1 is constant for any value of Vcontour. Specifically, if $R_{182} = R_{184}$ and $R_{188a} = R_{190a}$, then referring to equation (1), V_{bias} equals $-V_{contour}$ plus some constant voltage called K for clarity. If the wiper 154 is in the cutoff position (all the way toward the resistor 190a), then the voltage at the resistor 190a is $V_{bias} = (-V_{contour} + K)$ and the voltage at the resistor 188a is $V_{contour}$ regardless of the actual value of $V_{contour}$. Because the resistors 188a and 190a equal the same value R , then the current through the resistor 192a equals $(-V_{contour} + K)/R + V_{contour}/R = -K/R$. Thus, the cutoff value of Vgain-control1, which equals $K(R_{192a})/R$, is independent of $V_{contour}$. In one embodiment, K is selected such that the amplifier 198a generates the cutoff value of

Vgain-control1 high enough to ensure complete cutoff, *i.e.*, at least 90 to 100dB attenuation, of PGM1 as shown in Figures 11A – 11C.

The reversal circuit 144 operates in a manner similar to that discussed above in conjunction with Figure 12.

5 Although the operation of the crossfader circuit 106 is discussed with respect to the amplifier 198a and Vgain-control1, the operation with respect to the amplifier 198b and Vgain-control2 is similar.

FADER CONTROL CIRCUIT

10 Figure 14 is a block diagram of an embodiment of the gain core 99 and the fader control circuit 102 of Figure 6 where the circuit 102 combines the gain-control signals from the input-fader circuit 104 and the crossfader circuit 106 into a single gain-control signal for PGM1 and a single gain-control signal for PGM2. Thus, unlike prior-art fader control circuits that require multiple PGM1 and PGM2 amplifiers per
15 channel, the circuit 102 allows the use of only one amplifier per channel. This lowers cost and circuit complexity. Additionally, because active gain control elements have relatively high noise and/or distortion, performance is substantially improved by using only one gain control element per channel.

 The circuit 102 includes the input-fader circuit 104 of Figure 6, which is shown
20 as two circuits 104a and 104b for clarity — one for the PGM1 signal and the other for the PGM2 signal — and includes the crossfader circuit 106 of Figure 6. The circuit 102 also includes combiner circuits 200a and 200b, which combine the PGM1 input-fader and crossfader gain-control signals and the PGM2 input-fader and crossfader gain-control signals to generate the combined PGM1 and combined PGM2 gain-control signals, respectively. In one embodiment, the combiner circuits 200a and 200b are respective summers. The circuit 102 may also include low-pass filters 202a and 202b for reducing travel noise in the combined PGM1 and combined PGM2 gain-control signals, respectively. As discussed above in conjunction with
25 Figures 8 and 10, the input-fader and crossfader circuits 104 and 106 may include their own respective low-pass filters such that the circuits 202a and 202b can be
30 omitted. But an advantage of including them is that only two filters are needed, whereas four are needed if used in the input-fader and crossfader circuits, one each for the PGM1 and PGM2 gain-control signals generated by the input-fader circuit 104

and one each for the PGM1 and PGM2 gain-control signals generated by the crossfader circuit 106.

In one embodiment, the input-fader circuits 104a and 104b are the same as one of the embodiments of the input-fader circuit 104 discussed above in conjunction with Figures 6 and 8, and the crossfader circuit 106 is the same as one of the

embodiments discussed above in conjunction with Figures 6 and 10 - 13. Alternatively, the input-fader circuits 104a and 104b and the crossfader circuit 106 may be different than these previously described embodiments as long as they provide respective PGM1 and PGM2 input-fader and crossfader gain-control signals to the combiners 200a and 200b.

The gain core 99 includes one PGM1 amplifier 204a, which receives the combined PGM1 gain-control signal from the combiner 200a (via the low-pass filter 202a if included), and one PGM2 amplifier 204b, which receives the combined PGM2 gain-control signal from the combiner 200b (via the low-pass filter 202b if included). If the gain core 99 is designed for stereophonic signals, then it includes two amplifiers for PGM1, one for PGM1 L and one for PGM1 R, and two amplifiers for PGM2, one for PGM2 L and one for PGM2 R. Both of the PGM1 amplifiers receive the combined PGM1 gain-control signal, and both of the PGM2 amplifiers receive the combined PGM2 gain-control signal. The gain core 99 also includes a mixing circuit 205, which mixes the amplified PGM1 and PGM2 signals to generate the MASTER signal.

In operation, the input-fader circuits 104a and 104b respectively generate PGM1 and PGM2 input-fader gain-control signals, for example as discussed above in conjunction with Figure 8. Likewise, the crossfader circuit 106 generates PGM 1 and PGM 2 crossfader gain-control signals, for example the signals gain-control1 and gain-control2 as discussed above in conjunction with Figures 10 - 13. The combiner circuit 200a combines the PGM1 input-fader and crossfader gain-control signals to generate the combined PGM1 gain-control signal, and the combiner circuit 200b combines the PGM2 input-fader and crossfader gain-control signals to generate the combined PGM2 gain-control signal. The filters 202a and 202b filter the combined PGM1 and PGM2 gain-control signals to reduce travel noise as discussed above. The circuits 202a and 202b then provide these filtered gain-control signals to the amplifiers 204a and 204b. As discussed above, the combined

PGM1 and combined PGM2 gain-control signals control the gains of the amplifiers 204a and 204b, and thus to control the volumes and volume ratio of PGM1 and PGM2 in the MASTER signal. The mixer circuit 205 then mixes PGM1 and PGM2 from the amplifiers 204a and 204b, respectively, to generate the MASTER signal.

Figure 15 is a schematic diagram of an embodiment of the combiner circuits 200a and 200b, filters 202a and 202b, and the gain core 99 of Figure 14. A combination summer and filter circuit 206a performs the functions of the combining circuit 200a and the filter 202a, and a combination summer and filter circuit 206b performs the functions of the combining circuit 200b and the filter 202b. Specifically, the circuits 206a and 206b are summing integrators that add the PGM1 and PGM2 input-fader and crossfader gain-control signals together to generate the combined PGM1 and combined PGM 2 gain-control signals, respectively. The respective integration time constants of the circuits 206a and 206b are long enough to reduce travel noise but are short enough to avoid undesirable limiting of the maximum rate of change with respect to time of the combined PGM1 and combined PGM2 gain-control signals, respectively. That is, the circuits 206a and 206b effectively limit the rate at which the turntablist can vary the volumes of PGM1 and PGM2, but typically not to an extent that is noticeable to the turntablist. Furthermore, the circuits 206a and 206b symmetrically delay the respective attack and decay rates of the combined PGM1 and combined PGM2 gain-control signals. That is, the delay is substantially the same for both increases and decreases in the levels of these gain-control signals. Thus, the turntablist can count on the same volume response no matter which way he moves the input-fader and crossfader controls 66, 68, and 78 (e.g., Figure 5A). In one embodiment, the circuits 206a and 206b have respective corner frequencies in the range of approximately 10 – 50 Hz, for example approximately 45 Hz.

In this embodiment, the gain core 99 processes stereo signals, and includes voltage-controlled amplifiers 208a and 208b for PGM1 L and PGM1 R, respectively, and includes voltage-controlled amplifiers 210a and 210b for PGM2 L and PGM2 R, respectively. In this embodiment, the gains of these amplifiers is inversely proportional to the respective combined PGM1 and combined PGM2 gain-control signals. That is, as the gain-control voltage rises, the amplifier gain falls. In other embodiments, however, the amplifiers 208a, 208b, 210a, and 210b may have gains

that are proportional to the gain-control voltage, or may be current-controlled instead of voltage-controlled. The mixing circuit 205 includes a summer 212a for combining PGM1 L and PGM2 L into MASTER L, and includes a summer 212b for combining PGM1 R and PGM2 R into MASTER R.

Still referring to Figure 15, the values of the resistors and capacitors for one embodiment of the circuits 99 and 102 are as follows: $R1=1.1\text{ M}\Omega$, $R2=100\text{ k}\Omega$, $R3=30.1\text{ k}\Omega$, $R4=511\Omega$, $C1=.01\mu\text{F}$, $C2=470\text{pF}$, and $C3=47\text{pF}$. It is understood, however, that these values can be modified according to known circuit design principles to generate other embodiments of the invention.

TONE-CONTROL CIRCUIT

Figure 16 is a block diagram of an embodiment of the PGM1 tone-control circuit 97a of Figure 6, it being understood that the PGM2 tone-control circuit 97b is similar. For stereo signals, it is understood that there are four tone-control circuits that are similar to the circuit 97a, one each for PGM1 L, PGM1 R, PGM2 L, and PGM2 R.

In this embodiment, the PGM1 tone-control circuit 97a is a 4th-order tone-control circuit having three filter circuits: a 4th-order high-pass, *i.e.*, treble, filter circuit 220, a 4th-order band-pass, *i.e.*, mid-band, filter circuit 222, and a 4th-order low-pass, *i.e.*, bass, filter circuit 224. The filter circuits 220, 222, and 224 are coupled in parallel such that they each receive PGM1 and provide a respective filtered component of PGM1 to a combiner circuit 226, which combines the filtered components to generate PGM1 out. In one embodiment, the circuit 226 is a summer.

Each of the filter circuits 220, 222, and 224 has a Linkwitz-Riley alignment, which causes these filter circuits to have identical or nearly identical phase responses regardless of their respective gains. Thus, because the signals from these circuits all have the same or nearly the same phase, one can add these signals together to obtain a filtered PGM1 signal having little or no amplitude or phase distortion. That is, one can independently vary the respective gain of each filter path without significantly changing the phase response of that path, and thus without causing a significant amplitude error in the filtered PGM1 signal. The filter circuits 220, 222, and 224 also have the same or nearly the same respective corner

5 frequencies so that the tone-control circuit 97a has relatively stable and precise high and low corner frequencies. Thus, the tone-control circuit 97a provides steep cutoff slopes and allows independent gain control of the filtered bass-band, mid-band, and treble-band PGM1 components with fewer parts, a less complex design, and a smaller layout area than prior-art tone-control circuits.

10 In one embodiment, the treble filter circuit 220 includes two serially cascaded 2nd-order high-pass filters 228 and 230 in series with a gain-control circuit 232, which includes the treble gain control 58 (e.g., Figure 5A). Each of the filters 228 and 230 has a Butterworth alignment, and the serial combination of the filters 228 and 230 has a Linkwitz-Riley alignment such that the phase response of the filter circuit 220 is constant or nearly constant regardless of the setting of the treble control 58. Additionally, the filters 228 and 230 each have the same or nearly the same corner frequencies, and thus the filter circuit 220 has the same or nearly the same corner frequency as the filters 228 and 230.

15 In one embodiment, the mid-band filter circuit 222 includes a 4th-order low-pass filter 236 and a 4th-order high-pass filter 238, which are serially cascaded, and a gain-control circuit 240, which is in series with the filters 236 and 238 and which includes a mid-band gain control 241. Although the filter 236 is shown in front of the filter 238, the positions of these filters can be reversed without affecting the operation of the filter circuit 222. Each of the filters 236 and 238 has the Linkwitz-Riley alignment such that the phase response of the filter circuit 222 is constant or nearly constant regardless of the setting of the control 241 and is the same or nearly the same as the phase response of the treble filter circuit 220. The filters 236 and 238 have high and low corner frequencies, respectively, and the filter circuit 222 has the same or nearly the same high and low corner frequencies as the filters 236 and 238. Additionally, the high corner frequency of the filter 236, and thus the high corner frequency of the filter circuit 222, is the same or nearly the same as the corner frequency of the treble filter circuit 220.

25 In one embodiment, the low-pass filter 236 of the mid-band filter circuit 222 includes two serially cascaded 2nd-order low-pass filters 242 and 244, which each have the same or nearly the same high corner frequencies. Thus, the filter 236 and the filter circuit 222 have the same or nearly the same high corner frequency as the filters 242 and 244. Additionally, each of the filters 242 and 244 has the Butterworth

alignment, and the series combination of these filters has the Linkwitz-Riley alignment.

In one embodiment, the high-pass filter 238 of the mid-band filter circuit 222 includes two serially cascaded 2nd-order high-pass filters 246 and 248, which each have the same or nearly the same low corner frequencies. Thus the filter 238 and the filter circuit 222 have the same or nearly the same low corner frequency. Additionally, each of the filters 246 and 248 has the Butterworth alignment, and the series combination of these filters has the Linkwitz-Riley alignment.

In one embodiment, the bass filter circuit 224 includes two serially cascaded 2nd-order low-pass filters 250 and 252 in series with a gain-control circuit 254, which includes the bass gain control 56 (e.g., Figure 5A). Each of the filters 250 and 252 has the Butterworth alignment, and the serial combination of these filters has the Linkwitz-Riley alignment such that the phase response of the filter circuit 224 is constant or nearly constant regardless of the setting of the control 56, and is the same or nearly the same as the phase response of filter circuits 220 and 222. The filters 250 and 252 each have the same or nearly the same corner frequency, and thus the filter circuit 224 has the same or nearly the same corner frequency as the filters 250 and 252. Additionally, the corner frequency of filter 224 is the same or nearly the same as the low corner frequency of filter 222.

Figures 17 and 18 are Bode plots of the gain and phase responses of an embodiment of the tone-control circuit 97a of Figure 16 showing ranges of bass-band, mid-band, and treble-band gains. The gains of the filter circuits 220, 222, and 224 are or are approximately 6 dB down at their respective corner frequencies such that if each of these filter circuits has unity gain, the magnitudes of the filtered PGM1 components at the corner frequencies sum to approximately 0 dB such that the gain of the circuit 97a is substantially flat (at approximately 0dB) over the bass, mid, and treble-bands. One corner frequency of the circuit 97a, which is the same or nearly the same as the corner frequencies of the filter circuits 222 and 224, is within a range of 250 to 400 Hz, with a preferred value of 300 Hz. Similarly, the other corner frequency of the circuit 97a, which is the same or nearly the same as the corner frequencies of the filter circuits 220 and 222, is within a range of 3 to 5 kHz, with a preferred value of 4 kHz.

Referring to Figure 17, the circuit 97a provides steep cutoff slopes which allow isolation of a musical track such as a singing voice. Thus, these steep slopes allow the turntablist to cut or isolate the bass frequencies, which are typically below 300 Hz, the mid-band frequencies, which are typically in the range of 300 Hz to 4 kHz, or the treble frequencies, which are typically above 4 kHz, so that they are inaudible to a listener. For example, the frequencies in a human voice are typically between 500 Hz and 4 kHz. Thus, the turntablist can isolate a voice by putting the bass and treble controls 56 and 58 in their respective cutoff positions. This embodiment of the tone-control circuit 97a has cutoff slopes steep enough to provide approximately 40 dB of bass cut at 100 Hz and 40 dB of treble cut at 12 kHz as shown. These levels of cut are typically sufficient to isolate voice frequencies from bass and treble tracks. Furthermore, the bass and treble filter circuits 220 and 224 have maximum gains of approximately 10 dB, and the mid-band circuit 222 lacks the gain-control circuit 240 and thus has unity gain.

Still referring to Figure 17, the phase-response curve 260 is actually a representation of the overlapping phase-response curves of the filter circuits 220, 222, and 224. As shown, because the circuits 220, 222, and 224 have the Linkwitz-Riley alignment, they have the same or nearly the same phase response regardless of their respective gains.

Figure 18 is a Bode plot of an embodiment the circuit 97a of Figure 16 where the mid-band filter circuit 222 includes the gain-control circuit 240 and has a gain range of approximately +10 dB to -40 dB (the gain ranges of the treble and bass filter circuits 220 and 224 are omitted for clarity). Again, the steep cutoff slopes of the circuit 97a and the nearly identical phase responses of the filter circuits 220, 222, and 224 are evident.

Figure 19 is a schematic diagram of an embodiment of the tone-control circuit 97a of Figure 16 that provides gain and phase responses similar to those discussed above in conjunction with the Bode plot of Figure 17. In this embodiment, the mid-band filter circuit 222 does not include the gain-control circuit 240. In other embodiments, however, the circuit 222 includes a gain-control circuit 240 that is similar to the gain-control circuits 232 and 254. Furthermore, each of the filters 228, 230, 242, 244, 246, 248, 250, and 252 has a Sallen and Key topology and the Butterworth alignment, although in other embodiments these filters may have other

topologies or may not all have the same topology. Additionally, in one embodiment, the resistors and capacitors have the following values: R5=2.87 k Ω , R6=5.62 k Ω , R7=7.50 k Ω , R8=4.42 k Ω , R9=3.74 k Ω , R10=10.0 k Ω , R11=6.04 k Ω , R12=20.0 k Ω , R13=9.53 k Ω , R14=30.1 k Ω , C4=0.01 μ F, C5=0.0047 μ F, C6=0.1 μ F, C7=0.047 μ F, C8=82.0 pF, and C9=10.0 μ F. These values, however, may be changed according to established circuit-design principles to develop other embodiments of the invention.

Figure 20 is a block diagram of another embodiment of the tone-control circuit 97a of Figure 6, which filters PGM1 in the digital domain instead of in the analog domain. The circuit 97a includes an analog-to-digital (A/D) converter 260, which converts the PGM1_in analog signal into a PGM1dg_in digital signal. The circuit 97a also includes a digital signal processor (DSP) or other digital processing circuit 262, which digitally separates PGM1dg_in into its bass-band, mid-band, and treble-band components in a manner similar to that discussed above in conjunction with Figure 16. The DSP 262 combines these components to generate a digital output signal PGM1dg_out, which a digital-to-analog (D/A) converter 264 converts into the analog output signal PGM1_out. For example, the DSP 262 may sum the bass-band, mid-band, and treble-band components together to generate PGM1dg_out. Additionally, the circuit 97a includes treble-, bass-, and mid-band gain circuits 266, 268 and 270, which allow the turntablist to independently adjust the amplitudes of the bass-band, mid-band, and treble-band components, respectively, of PGM1dg_in. Although the A/D and D/A converters 260 and 264 are shown separate from the DSP 262, in other embodiments the DSP 262 incorporates one or both of the A/D and D/A converters 260 and 264.

Figure 21 is a block diagram of another embodiment of the PGM1 tone-control circuit 97a of Figure 6, it being understood that the PGM2 tone-control circuit 97b is similar. For stereo signals, it is understood that there are four tone-control circuits that are similar to the circuit 97a, one each for PGM1 L, PGM1 R, PGM2 L, and PGM2 R.

In this embodiment, the PGM1 tone-control circuit 97a is a 2nd-order tone-control circuit having three filter circuits: a 2nd-order high-pass, *i.e.*, treble, filter circuit 280, a 2nd-order band-pass, *i.e.*, mid-band, filter circuit 282, and a 2nd-order low-

pass, *i.e.*, bass, filter circuit 284. Like the filter circuits 220, 222, and 224 of Figure 16, the filter circuits 280, 282, and 284 are coupled in parallel such that they each receive PGM1 and provide a respective filtered component of PGM1 to a combiner circuit 300, which combines the filtered components to generate PGM1_out. In one embodiment, the circuit 300 is a summer.

Each of the filter circuits 280, 282, and 284 has the Linkwitz-Riley alignment such that they have the same or nearly the same phase response. The filter circuits 280, 282, and 284 also have the same or nearly the same respective corner frequencies so that the tone-control circuit 97a has relatively stable and precise high and low corner frequencies. Thus, the 2nd-order tone-control circuit 97a provides steep cutoff slopes and allows independent gain control of the filtered bass-band, mid-band, and treble-band PGM1 components with fewer parts, a less complex design, and a smaller layout area than prior-art tone-control circuits and the tone-control circuit 97a of Figure 16.

The treble filter circuit 280 includes a 2nd-order high-pass filter 286 in series with a gain-control circuit 288, which includes the treble control 58 (e.g., Figure 5A). The filter 286 has the Linkwitz-Riley alignment, and its corner frequency is the corner frequency of the filter circuit 280.

The mid-band filter circuit 282 includes a 2nd-order high-pass filter 290 and a 2nd-order low-pass filter 292, which are serially cascaded, and an optional gain-control circuit 294, which is in series with the filters 290 and 292 and which includes the mid-band gain control 241. Each of the filters 290 and 292 has the Linkwitz-Riley alignment. Although the filter 290 is shown in front of the filter 292, the positions of these filters can be reversed without affecting the operation of the filter circuit 282.

The corner frequencies of the filters 290 and 292 are the low and high corner frequencies, respectively, of the filter circuit 282, and the corner frequency of the filter 292 is the same or nearly the same as the corner frequency of the treble filter circuit 280. In one embodiment, the filter 290 has a non-inverting topology and the filter 292 has an inverting topology. In another embodiment, however, the filter 290 has an inverting topology and the filter 292 has a non-inverting topology. In yet another embodiment, both of the filters 290 and 292 have either inverting or non-inverting topologies and are in series with an inverter (not shown) to give the proper phase characteristics to the mid-band filter circuit 282.

The bass filter circuit 284 includes a 2nd-order low-pass filter 296 in series with a gain-control circuit 298, which includes the bass control 56 (e.g., Figure 5A). The filter 296 has the Linkwitz-Riley alignment, and its corner frequency is the corner frequency of the filter circuit 284 and is the same or nearly the same as the low corner frequency of the filter circuit 282.

In operation, the 2nd-order tone-control circuit 97a operates in a manner similar to that described in conjunction with Figure 16 for the 4th-order tone-control circuit 97a. Because this tone-control circuit 97a is of the 2nd order, it includes significantly fewer components than the 4th-order tone-control circuit of Figure 16. Thus, the 2nd-order tone-control circuit 97a of Figure 21 occupies less circuit-board area and is significantly less expensive than the 4th-order tone-control circuit of Figure 16.

Figures 22 and 23 are Bode plots of the gain and phase responses of an embodiment of the 2nd-order tone-control circuit 97a of Figure 21 for ranges of the bass-band, mid-band, and treble-band gains. The gains of the filter circuits 280, 282, and 284 are or are approximately 6 dB down at their respective corner frequencies such that if each of the filters circuits has unity gain, the magnitudes of the filtered PGM1 components at the corner frequencies sum to approximately 0 dB such that the gain of the circuit 97a is substantially flat (at approximately 0dB) over the bass-, mid-, and treble-bands. The low corner frequency of the circuit 97a is within a range of 250 to 400 Hz, with a preferred value of 300 Hz. Similarly, the high corner frequency of the circuit 97a is within a range of 3 to 5 kHz with a preferred value of 4 kHz. Referring to Figure 22, the 2nd-order circuit 97a thus provides steep cutoff slopes — although not as steep as the cutoff slopes of the 4th-order circuit 97a of Figure 16 — that allow reasonable isolation of a musical track such as a singing voice. This embodiment of 2nd-order tone-control circuit 97a has cutoff slopes steep enough to provide approximately 20 dB of bass cut at 100 Hz and 20 dB of treble cut at 12 kHz. Furthermore, the bass and treble filter circuits 280 and 284 have maximum gains of approximately 10 dB, and the mid-band circuit 282 lacks the gain-control circuit 294 and thus has unity gain.

Still referring to Figure 22, the phase-response curve 308 is a representation of the overlapping phase-response curves of the filter circuits 280, 282, and 284. As shown, because the filter circuits 280, 282, and 284 have the Linkwitz-Riley

alignment, they have the same or nearly the same phase response regardless of their respective gains.

Figure 23 is a Bode plot of an embodiment the 2nd-order tone-control circuit 97a of Figure 21 where the mid-band filter circuit 282 includes the gain-control circuit 294 and has a gain range of approximately +10 dB to -20 dB. Again, the steep cutoff slopes of the 2nd-order circuit 97a and the nearly identical phase responses of the filter circuits 280, 282, and 284 are evident.

Figure 24 is a schematic diagram of the embodiment of the filter circuits 280, 282, and 284 that provides the gain and phase responses shown in Figures 22 and 23. In this embodiment, the filters 286, 290, and 296 each have the Sallen and Key topology, and the filter 292 has an inverting multiple-feedback topology. In another embodiment, however, the filter 290 has the inverting multiple-feedback topology and the filter 292 has the Sallen and Key topology. In yet another embodiment, both the filters 290 and 292 have either an inverting multiple-feedback topology or a Sallen and Key topology and are in series with an inverter (not shown). Either way, the mid-band filter circuit 282 has an odd number of inversions to give it a proper phase shift. Furthermore, like the high-pass filter 286 and the low-pass filter 296, the high-pass filter 290 and the low-pass filter 292 each have the Linkwitz-Riley alignment. Additionally, in one embodiment, the resistor and capacitor values are as follows: R15=4.02 kΩ, R16=5.36 kΩ, R17=1.91 kΩ, R18=19.1 kΩ, C10=0.01 μF, C11=0.1 μF, C12=0.022 μF, and C13=0.001μF. These values, however, may be changed according to established circuit-design principles to develop other embodiments of the invention.

Referring to Figures 20 and 24, an embodiment of the 2nd-order tone-control circuit 97a of Figure 21 is implement digitally using the same basic components and theory of operation as discussed in conjunction with Figure 20. In this embodiment, the DSP 262 is programmed to digitally implement 2nd-order bass-, mid-, and treble-band filters having characteristics similar to those described above in conjunction with Figures 21 – 24 for the filter circuits 280, 282, and 284.

AUDIO-EFFECTS MULTIPLEXER

Figure 25 is a functional diagram of an embodiment of the effects-path multiplexer 98a of Figure 7A, an effects connector 322, and a switch circuit 320,

which generates a path-selection signal based on the settings of the controls 84 and 86 of Figure 7A. For clarity, only the portion 98a (Figure 7A) of the multiplexer 98 (Figure 6) associated with PGM1 L, PGM2 L, and MASTER L is shown, it being understood that the portion 98b for PGM1 R, PGM2 R, and MASTER R is similar.

5 The portion 98a includes three input terminals 326, 328, and 330 for respectively receiving PGM1 Lin, PGM2 Lin, and MASTER Lin, and includes three output terminals 332, 334, and 336 for respectively providing PGM1 Lout, PGM2 Lout, and MASTER Lout. The multiplexer portion 98a also includes a switching circuit 338 for routing the input signals in response to the selection signal from the

10 switch circuit 320.

In operation, the turntablist sets the controls 84 and 86 to route the desired one of the input signals PGM1 Lin, PGM2 Lin, and MASTER Lin through the effects box 18 (e.g., Figure 5D). Alternatively, the turntablist may choose to route none of these input signals through the effects box 18. In the illustrated mode of operation,

15 the switch circuit 320 provides the selection signal having a value that causes the switching circuit 338 to route PGM1 Lin from the input terminal 326, through the effects box 18, and to the output terminal 332 as PGM1 Lout. This value of the selection signal also causes the switching circuit 338 to route the signals PGM2 Lin and MASTER Lin from the input terminals 328 and 330 directly to the corresponding

20 output terminals 334 and 336, respectively. Thus, in this mode, PGM2 Lin and MASTER Lin pass through the multiplexer 98 essentially unaltered. In other modes of operation, the selection signal has respective values that cause the switching circuit 338 to route PGM2 Lin and MASTER Lin through the effects box 18 in a similar manner. Thus, in this embodiment, the switching circuit 338 routes no more

25 than one signal through the effects box 18 at a time. In yet another mode of operation, the selection signal has a value that causes the switching circuit 338 to route none of the signals through the effects box 18. Thus, in this mode, the switching circuit 338 couples the input terminals 326, 328, and 330 directly to the output terminals 332, 334, and 336, respectively.

30 Still referring to Figure 25, the connector 322, includes a safeguard mechanism 324, which prevents the turntablist from unintentionally cutting off one of the input signals PGM1 Lin, PGM2 Lin, and MASTER Lin. Specifically, if an effects-box connector (not shown) is connected to the connector 322, the mechanism 324

acts as an open switch between the effects input and output terminals (Effects in, Effects out) of the multiplexer 98a. But if no connector is connected to the connector 322, then the mechanism 324 acts as a closed switch such that the effects input and output terminals are coupled together. Thus, if the effects box 18 (Figure 5D) is not connected to the mixer 50 (Figure 5D) and the turntablist accidentally adjusts the controls 84 and 86 to route a signal through the effects box 18, the mechanism 324 acts as a short circuit and routes the signal to the proper output terminal 322, 324, or 326. Without the mechanism 324, the path of the signal inadvertently routed to the effects output terminal would be electrically open, thus cutting off a portion of MASTER Lout if PGM1 Lin or PGM2 Lin is inadvertently routed or completely cutting off MASTER Lout if MASTER Lin is inadvertently routed.

Although the controls 84 and 86 and the switching mechanism 324 are described as mechanical switching components, in other embodiments they are electrical or optical components.

Figures 26A and 26B are a schematic diagram of an embodiment of the effects multiplexer 98 of Figure 6 including the portions 98a and 98b, which are similar to the portions 98a and 98b described in conjunction with Figure 25. Referring to Figure 26A, the switch circuit 320 includes two switch sub circuits 340 and 342, which respectively include the switches 86 and 84. The switch circuit 320 also includes a logic circuit 344, which generates components 346 of the selection signal in response to the positions of the switches 84 and 86. Referring to Figure 26B, the multiplexer 98 also includes a bank of analog input switches 348, which couple the respective input signals either to the effects output terminal or to a respective output terminal 332, 334, or 336. For clarity, these output terminals are shown in two places: at the respective outputs of the switches 348 and at the respective outputs of a selector 354, it being understood that these are the same respective output terminals in an electrical sense. The multiplexer 98 also includes output buffer circuits 350L and 350R, which buffer the respective L and R components of selected input signal that is routed to the effects output terminal (send), and includes input buffer circuits 352L and 352R, which buffer the respective L and R components of the selected signal as it returns from the effects box 18 (e.g., Figure 5D) at the effects input terminal (return). Additionally, the multiplexer 98

includes the selector 354, which couples the components of the returned signal from the buffer circuits 352 to the appropriate output terminals.

In operation, for the positions of the switches 84 and 86 illustrated in Figure 26A, the logic circuit 344 generates the selection-signal components P1D, P2D, and MD equal to logic 1, and the components P1S, P2S, and MS equal to logic 0.

Therefore, the switches 348a, 348c, 348e, 348g, 348i, and 348k are closed, and the switches 348b, 348d, 348f, 348h, 348j, and 348l are open such that none of the input signals PGM1 L and R, PGM2 L and R, and MASTER L and R are routed through the effects box 18 (e.g., Figure 5D). Furthermore, the circuit 344 generates values for the components A0 and A1 such that the selector 354 isolates the effects box 18 from the output terminals 332L, 332R, 334L, 334R, 336L, and 336R.

If, however, the switches 84 and 86 are in other positions, the logic circuit 344 generates a respective one of the signals P1D, P2D, or MD equal to logic 0 and the corresponding one of the signals P1S, P2S, and MS equal to logic 1 such that the switches 348 route a selected one of the input signals through the effects box 18.

Furthermore the circuit 344 generates values for the components A0 and A1 such that the selector 354 routes the signal returned from the effects box 18 to the proper output terminal 332, 334, or 336. For example, to route PGM1 L and PGM1 R through the effects box 18, the turntablist puts the switches 84 and 86 in respective positions such that the logic circuit generates P1D equal to logic 0, P1S equal to logic 1, P2D and MD equal to logic 1, and P2S and MS equal to logic 0. These values close the switches 348b and 348h to respectively couple PGM1 L and PGM1 R to the buffers 350L and 350R, close the switches 348c, 348e, 348i, and 348k to couple PGM2 L, PGM2 R, MS L, and MS R directly to the respective output terminals 334L, 334R, 336L, and 336R, and open the remaining switches 348.

Furthermore, the circuit 344 generates the values of A0 and A1 such that the selector 354 couples the left return signal from the buffer 352L to the output terminal 332L and couples the right return signal from the buffer circuit 352R to the output terminal 332R.

Although described as routing at most only one signal PGM1, PGM2, or MASTER at a time to the effects box 18 (Figure 5D), other embodiments of the mixer 50 and multiplexer 98 allow the simultaneous routing of multiple signals to one or more effects boxes. Furthermore, in one embodiment, the resistors and capacitors

have the following values: R19=10 k Ω , R20=511 Ω , R21=100 k Ω , R22=301 Ω , R23=20 k Ω , R24=1 k Ω , C14>10 μ F, C15=47pF, and C16=330pF. It is understood, however, that these values may be changed according to established circuit-design principals to develop other embodiment of the invention.

- 5 From the foregoing it will be appreciated that, although specific embodiments of the invention have been described herein for purposes of illustration, various modifications may be made without deviating from the spirit and scope of the invention.

10

What is claimed:

1. An audio-signal circuit, comprising:

a 4th-order low-pass filter circuit having a first phase response and operable to receive and filter an audio signal and to generate a first output signal;

5 a 4th-order band-pass filter circuit having a second phase response substantially equal to the first phase response and operable to receive and filter the audio signal to generate a second output signal;

10 a 4th-order high-pass filter circuit having a third phase response substantially equal to the first and second phase responses and operable to receive and filter the audio signal to generate a third output signal; and

a combining circuit coupled to the low-pass, band-pass, and high-pass filter circuits and operable to combine the first, second, and third output signals into a combined signal.

15 2. The audio-signal circuit of claim 1 wherein the low-pass, band-pass, and high-pass filter circuits each have a Linkwitz-Riley alignment.

3. The audio-signal circuit of claim 1 wherein:

the low-pass filter circuit has a first cutoff frequency;

20 the band-pass filter circuit has the first cutoff frequency and has a second cutoff frequency that is higher than the first cutoff frequency; and

the high-pass filter circuit has the second cutoff frequency.

4. The audio-signal circuit of claim 1 wherein:

25 the low-pass filter circuit has a first cutoff frequency and a first gain that is –6dB at the first cutoff frequency;

the band-pass filter circuit has the first cutoff frequency, a second cutoff frequency that is higher than the first cutoff frequency, and a second gain that is –6dB at the first and second cutoff frequencies; and

30 the high-pass filter circuit has the second cutoff frequency and a third gain that is –6dB at the second cutoff frequency.

5. The audio-signal circuit of claim 1 wherein:
the low-pass filter circuit has a gain of approximately -40dB at 100 Hz; and
the high-pass filter circuit has a gain of approximately -40dB at 12 kHz.

5 6. The audio-signal circuit of claim 1 wherein:
the low-pass, band-pass, and high-pass filter circuits have respective first,
second, and third gains; and
the first, second, and third phase responses of the low-pass, band-pass, and
high-pass filter circuits are respectively independent of the first, second, and third
10 gains.

7. The audio-signal circuit of claim 1 wherein the combining circuit is
operable to sum together the first, second, and third output signals to generate the
combined signal.

15 8. The audio-signal circuit of claim 1 wherein the low-pass, band-pass,
and high-pass filter circuits comprise respective digital filters.

20 9. An audio-signal circuit, comprising:
audio input and output terminals;
a first series combination of two 2^{nd} -order low-pass filters, the series
combination having a first phase response, an input terminal coupled to the audio
input terminal, and an output terminal;
a second series combination of two 2^{nd} -order low-pass filters and two 2^{nd} -
25 order high-pass filters, the second series combination having a second phase
response substantially equal to the first phase response, an input terminal coupled to
the audio input terminal, and an output terminal;
a third series combination of two 2^{nd} -order high-pass filters, the third series
combination having a third phase response substantially equal to the first and
30 second phase responses, an input terminal coupled to the audio input terminal, and
an output terminal; and

a combining circuit having first, second, and third input terminals respectively coupled to the output terminals of the first, second, and third series combinations and having an output terminal coupled to the audio output terminal.

5 10. The audio-signal circuit of claim 9 wherein each filter of the first, second, and third series combinations has a Butterworth alignment.

11. The audio-signal circuit of claim 9 wherein the first series combination of the low-pass filters, the combination of the two low-pass filters and the
10 combination of the two high-pass filters in the second series combination, and the third series combination of the high-pass filters each have a Linkwitz-Riley alignment.

12. The audio-signal circuit of claim 9 wherein:
15 the first series combination has a first cutoff frequency;
the second series combination has the first cutoff frequency and has a second cutoff frequency that is higher than the first cutoff frequency; and
the third series combination has the second cutoff frequency.

20 13. The audio-signal circuit of claim 9 wherein:
the first series combination has a cutoff frequency within a first range of approximately 250 – 400 Hz;
the second series combination has a first cutoff frequency within the first range and has a second cutoff frequency within a second range of approximately 3 –
25 5 kHz; and
the third series combination has a cutoff frequency within the second range.

14. The audio-signal circuit of claim 9 wherein:
the first series combination has a cutoff frequency of approximately 300 Hz;
30 the second series combination has a first cutoff frequency of approximately 300 Hz and has a second cutoff frequency of approximately 4 kHz; and
the third series combination has a cutoff frequency of approximately 4 kHz.

15. The audio-signal circuit of claim 9 wherein:
the first series combination has a first cutoff frequency and a first gain that is –
6dB at the first cutoff frequency;
the second series combination has the first cutoff frequency, a second cutoff
5 frequency that is higher than the first cutoff frequency, and a second gain that is –
6dB at the first and second cutoff frequencies; and
the third series combination has the second cutoff frequency and a third gain
that is –6dB at the second cutoff frequency.

10 16. The audio-signal circuit of claim 9 wherein:
the first series combination has a gain of approximately –40dB at 100 Hz; and
the third series combination has a gain of approximately –40dB at 12 kHz.

15 17. The audio-signal circuit of claim 9 wherein:
the first series combination includes a gain control coupled in series with its
two low-pass filters; and
the third series combination includes a gain control coupled in series with its
two high-pass filters.

20 18. The audio-signal circuit of claim 9 wherein the second series
combination includes a gain control coupled in series with its two low-pass and two
high-pass filters.

25 19. The audio-signal circuit of claim 9 wherein each filter of the first,
second, and third series combinations has a Sallen and Key topology.

20. The audio-signal circuit of claim 9 wherein:
the first, second, and third series combinations have respective first, second,
and third gains; and
30 the first, second, and third phase responses of the first, second, and third
series combinations are respectively independent of the first, second, and third
gains.

21. The audio-signal circuit of claim 9 wherein the combining circuit comprises a summer.

22. The audio-signal circuit of claim 9 wherein the two 2nd-order low-pass filters of the first series combination, the two 2nd-order low-pass filters and the two 2nd-order high-pass filters of the second series combination, and the two 2nd-order high-pass filters of the third series combination comprise respective digital filters.

23. An audio-signal circuit, comprising:
a 2nd-order low-pass filter circuit having a first phase response and operable to receive and filter an audio signal and to generate a first output signal;
a 2nd-order band-pass filter circuit having a second phase response substantially equal to the first phase response and operable to receive and filter the audio signal to generate a second output signal;
a 2nd-order high-pass filter circuit having a third phase response substantially equal to the first and second phase responses and operable to receive and filter the audio signal to generate a third output signal; and
a combining circuit coupled to the low-pass, band-pass, and high-pass filter circuits and operable to combine the first, second, and third output signals into a combined signal.

24. The audio-signal circuit of claim 23 wherein the low-pass, band-pass, and high-pass filter circuits each have a Linkwitz-Riley alignment.

25. The audio-signal circuit of claim 23 wherein:
the low-pass filter circuit has a first cutoff frequency;
the band-pass filter circuit has the first cutoff frequency and has a second cutoff frequency that is higher than the first cutoff frequency; and
the high-pass filter circuit has the second cutoff frequency.

26. The audio-signal circuit of claim 23 wherein:
the low-pass filter circuit has a first cutoff frequency and a first gain that is – 6dB at the first cutoff frequency;

the band-pass filter circuit has the first cutoff frequency, a second cutoff frequency that is higher than the first cutoff frequency, and a second gain that is –6dB at the first and second cutoff frequencies; and

5 the high-pass filter circuit has the second cutoff frequency and a third gain that is –6dB at the second cutoff frequency.

27. The audio-signal circuit of claim 23 wherein:

the low-pass filter circuit has a gain of approximately –20dB at 100 Hz; and

the high-pass filter circuit has a gain of approximately –20dB at 12 kHz.

10

28. The audio-signal circuit of claim 23 wherein:

the low-pass, band-pass, and high-pass filter circuits have respective first, second, and third gains; and

15 the first, second, and third phase responses of the low-pass, band-pass, and high-pass filter circuits are respectively independent of the first, second, and third gains.

29. The audio-signal circuit of claim 23 wherein the combining circuit is operable to sum together the first, second, and third output signals to generate the combined signal.

20

30. The audio-signal circuit of claim 23 wherein:

the low-pass filter circuit comprises a 2nd-order low-pass filter;

the band-pass filter circuit comprises a series combination of a 2nd-order low-pass filter and a 2nd-order high-pass filter; and

25

the high-pass filter circuit comprises a 2nd-order high-pass filter.

31. The audio-signal circuit of claim 23 wherein the low-pass, band-pass, and high-pass filter circuits comprise respective digital filters.

30

32. An audio-signal circuit, comprising:

audio input and output terminals;

a 2nd-order low-pass filter that has a first phase response, an input terminal coupled to the audio input terminal, and an output terminal;

a series combination of a 2nd-order low-pass filter and a 2nd-order high-pass filter, the series combination having a second phase response substantially equal to the first phase response, an input terminal coupled to the audio input terminal, and an output terminal; and

a 2nd-order high-pass filter that has a third phase response substantially equal to the first and second phase responses, an input terminal coupled to the audio input terminal, and an output terminal; and

a combining circuit having first, second, and third input terminals respectively coupled to the output terminals of the low-pass filter, series combination of low-pass and high-pass filters, and high-pass filter and having an output terminal coupled to the audio output terminal.

33. The audio-signal circuit of claim 32 wherein:
the low-pass filter, the low-pass and high-pass filters of the series combination, and the high-pass filter each have a Linkwitz-Riley alignment.

34. The audio-signal circuit of claim 32 wherein:
the low-pass filter, the low-pass and high-pass filters of the series combination, and the high-pass filter each have a Linkwitz-Riley alignment; and
one of the low-pass and high-pass filters of the series combination has an inverting topology.

35. The audio-signal circuit of claim 32 wherein:
the low-pass filter, the low-pass and high-pass filters of the series combination, and the high-pass filter each have a Linkwitz-Riley alignment; and
one of the low-pass and high-pass filters of the series combination has an inverting multiple-feedback topology.

36. The audio-signal circuit of claim 32 wherein:
the low-pass filter has a first cutoff frequency;

the series combination of the low-pass and high-pass filters has the first cutoff frequency and has a second cutoff frequency that is higher than the first cutoff frequency; and

the high-pass filter has the second cutoff frequency.

5

37. The audio-signal circuit of claim 32 wherein:

the low-pass filter has a cutoff frequency within a first range of approximately 250 – 400 Hz;

the series combination of the low-pass and high-pass filters has a first cutoff frequency within the first range and has a second cutoff frequency within a second range of approximately 3 – 5 kHz; and

the high-pass filter has a cutoff frequency within the second range.

10

38. The audio-signal circuit of claim 32 wherein:

the low-pass filter circuit has a cutoff frequency of approximately 300 Hz;

the series combination of the low-pass and high-pass filters has a first cutoff frequency of approximately 300 Hz and has a second cutoff frequency of approximately 4 kHz; and

the high-pass filter has a cutoff frequency of approximately 4 kHz.

15

20

39. The audio-signal circuit of claim 32 wherein:

the low-pass filter has a first cutoff frequency and a first gain that is –6dB at the first cutoff frequency;

25

the series combination of the low-pass and high-pass filters has the first cutoff frequency, a second cutoff frequency that is higher than the first cutoff frequency, and a second gain that is –6dB at the first and second cutoff frequencies; and

the high-pass filter circuit has the second cutoff frequency and a third gain that is –6dB at the second cutoff frequency.

30

40. The audio-signal circuit of claim 32 wherein:

the low-pass filter has a gain of approximately –20dB at 100 Hz; and

the high-pass filter has a gain of approximately –20dB at 12 kHz.

41. The audio-signal circuit of claim 32, further comprising:
a low-pass gain control coupled in series with the low-pass filter; and
a high-pass gain control coupled in series with the high-pass filter.

5 42. The audio-signal circuit of claim 32, further comprising a gain control
coupled in series with the low-pass and high-pass filters of the series combination.

43. The audio-signal circuit of claim 32 wherein each of the low-pass and
high-pass filters and one of the filters of the series combination has a Sallen and Key
10 topology.

44. The audio-signal circuit of claim 32 wherein:
the low-pass, high-pass, and series combination of low-pass and high-pass
filters have respective first, second, and third gains; and
15 the first, second, and third phase responses are respectively independent of
the first, second, and third gains.

45. The audio-signal circuit of claim 32 wherein the combining circuit
comprises a summing circuit.
20

46. The audio-signal circuit of claim 32 wherein the low-pass filter, the low-
pass and high-pass filters of the series combination, and the high-pass filter
comprise respective digital filters.

25 47. An audio circuit, comprising:
an analog-to-digital converter operable to receive an analog audio signal
having a range of frequencies and to convert the analog signal into a digital audio
signal;
a processor coupled to the converter, operable to filter the digital audio signal,
30 operable to generate first, second, and third filtered digital signals that each include
respective first, second, and third portions of the range of frequencies of the audio
signal, and operable to combine the first, second, and third filtered digital signals into
a combined filtered digital signal; and

a digital-to-analog converter coupled to the processor and operable to convert the combined filtered digital signal into a combined filtered analog signal.

48. The audio circuit of claim 47 wherein the processor is operable to
5 generate the first, second, and third filtered digital signals by filtering the digital audio signal with first, second, and third 2nd-order filter functions.

49. The audio circuit of claim 47 wherein the processor is operable to
10 generate the first, second, and third filtered digital signals by filtering the digital audio signal with first, second, and third 4th-order filter functions.

50. The audio circuit of claim 47 wherein the first, second, and third filtered
15 digital signals respectively comprise the bass-band, mid-band, and treble-band portions of the audio signal.

51. A method, comprising:

filtering an audio signal with a 4th-order low-pass filter circuit to generate a first
output signal, the low-pass filter having a first phase response;

20 filtering the audio signal with a 4th-order band-pass filter circuit to generate a second output signal, the band-pass filter circuit having a second phase response substantially equal to the first phase response;

filtering the audio signal with a 4th-order high-pass filter to generate a third
output signal, the high-pass filter circuit having a third phase response substantially
equal to the first and second phase responses; and

25 combining the first, second, and third output signals into a combined signal.

52. The method of claim 51 wherein each of the low-pass, band-pass, and
high-pass filter circuits has a Linkwitz-Riley alignment.

30 53. The method of claim 51, further comprising changing the respective gains of the low-pass and high-pass filter circuits without significantly changing the first and third phase responses.

54. The method of claim 51, further comprising changing the gain of the band-pass filter circuit without significantly changing the second phase response.

55. The method of claim 51, further comprising simultaneously filtering the
5 audio signal with the low-pass, band-pass, and high-pass filter circuits.

56. The method of claim 51 wherein the combining comprises summing together the first, second, and third output signals to generate the combined signal.

10 57. The method of claim 51 wherein the low-pass, band-pass, and high-pass filters comprise analog filtering circuitry.

58. The method of claim 51 wherein the low-pass, band-pass, and high-pass filters comprise digital filtering circuitry.

15 59. A method, comprising:
filtering an audio signal with a 2nd-order low-pass filter circuit to generate a first output signal, the low-pass filter having a first phase response;
filtering the audio signal with a 2nd-order band-pass filter circuit to generate a
20 second output signal, the band-pass filter circuit having a second phase response substantially equal to the first phase response;
filtering the audio signal with a 2nd-order high-pass filter to generate a third output signal, the high-pass filter circuit having a third phase response substantially equal to the first and second phase responses; and
25 combining the first, second, and third output signals into a combined signal.

60. The method of claim 59 wherein each of the low-pass, band-pass, and high-pass filter circuits has a Linkwitz-Riley alignment.

30 61. The method of claim 59, further comprising changing the respective gains of the low-pass and high-pass filter circuits without significantly changing the first and third phase responses.

62. The method of claim 59, further comprising changing the gain of the band-pass filter circuit without significantly changing the second phase response.

5 63. The method of claim 59, further comprising simultaneously filtering the audio signal with the low-pass, band-pass, and high-pass filter circuits.

64. The method of claim 59 wherein the combining comprises summing together the first, second, and third output signals to generate the combined signal.

10 65. The method of claim 59 wherein the low-pass, band-pass, and high-pass filters comprise analog filtering circuitry.

66. The method of claim 59 wherein the low-pass, band-pass, and high-pass filters comprise digital filtering circuitry.

ABSTRACT

An audio tone-control circuit includes 4th-order low-pass, 4th-order band-pass, and 4th-order high-pass filter circuits. The 4th-order low-pass filter circuit has a first phase response and receives and filters an audio signal and generates a first output signal therefrom. The 4th-order band-pass filter circuit has a second phase response that is substantially equal to the first phase response and receives and filters the audio signal to generate a second output signal. The 4th-order high-pass filter circuit has a third phase response substantially equal to the first and second phase responses and receives and filters the audio signal to generate a third output signal. The audio-signal circuit also includes a combining circuit that combines the first, second and third output signals into a combined signal. Furthermore, the filter circuits may be 2nd-order filter circuits instead of 4th-order filter circuits.

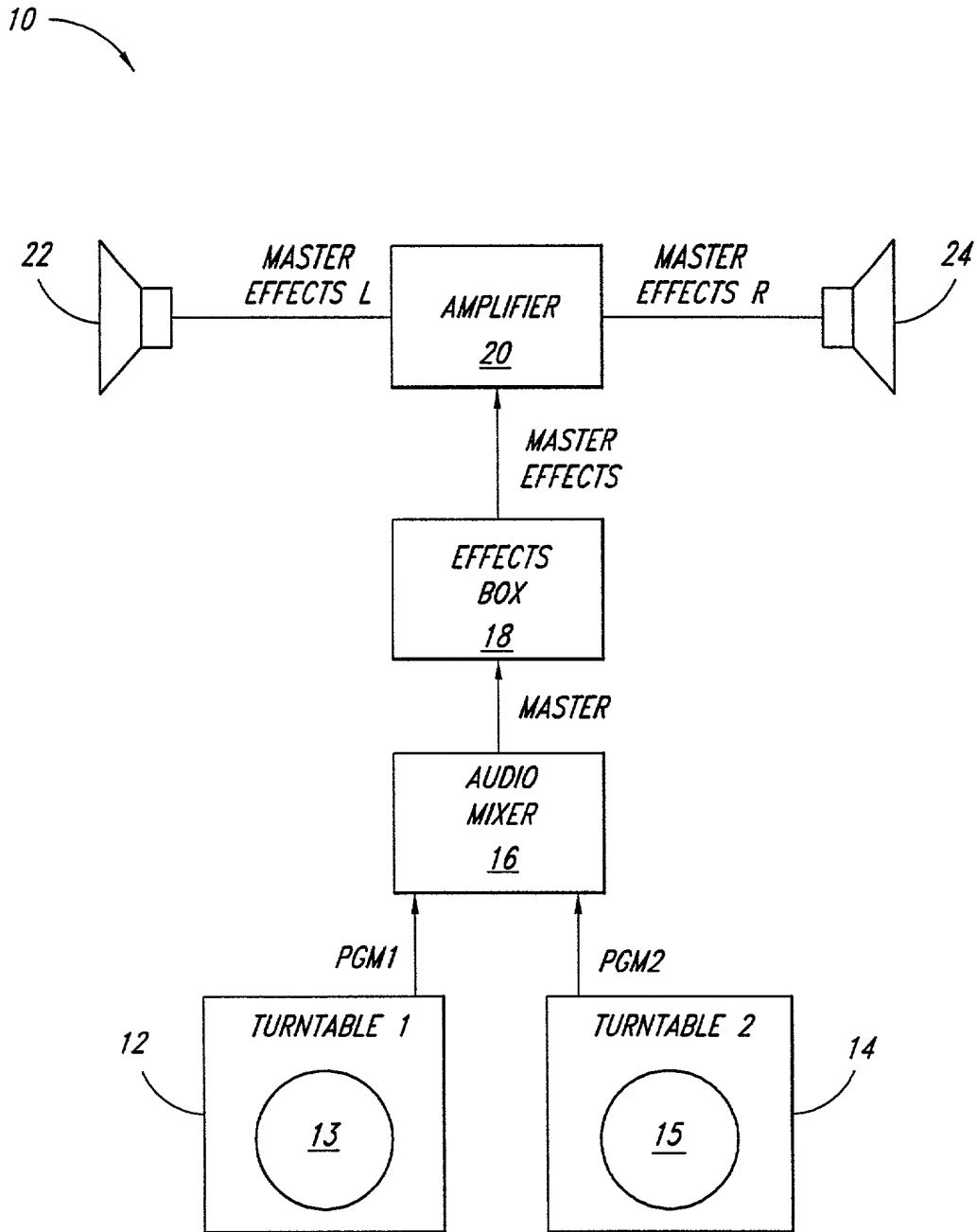


Fig. 1 (PRIOR ART)

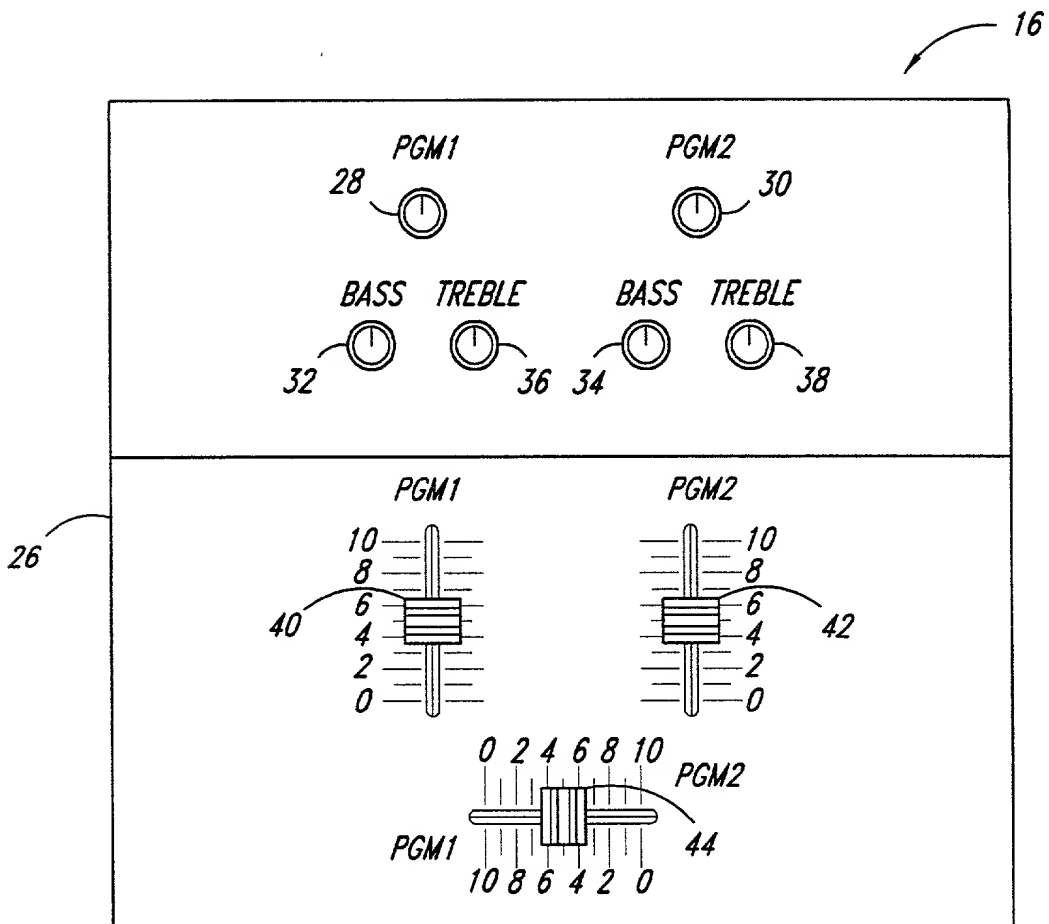


Fig. 2 (PRIOR ART)

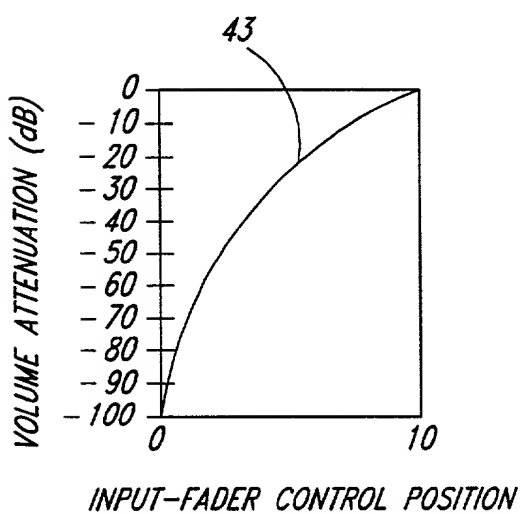


Fig. 3 (PRIOR ART)

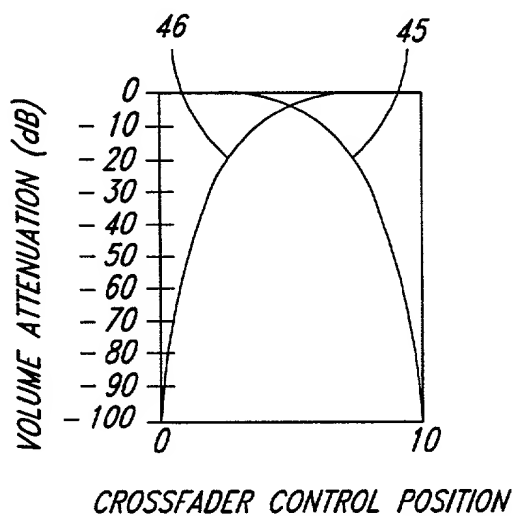


Fig. 4 (PRIOR ART)

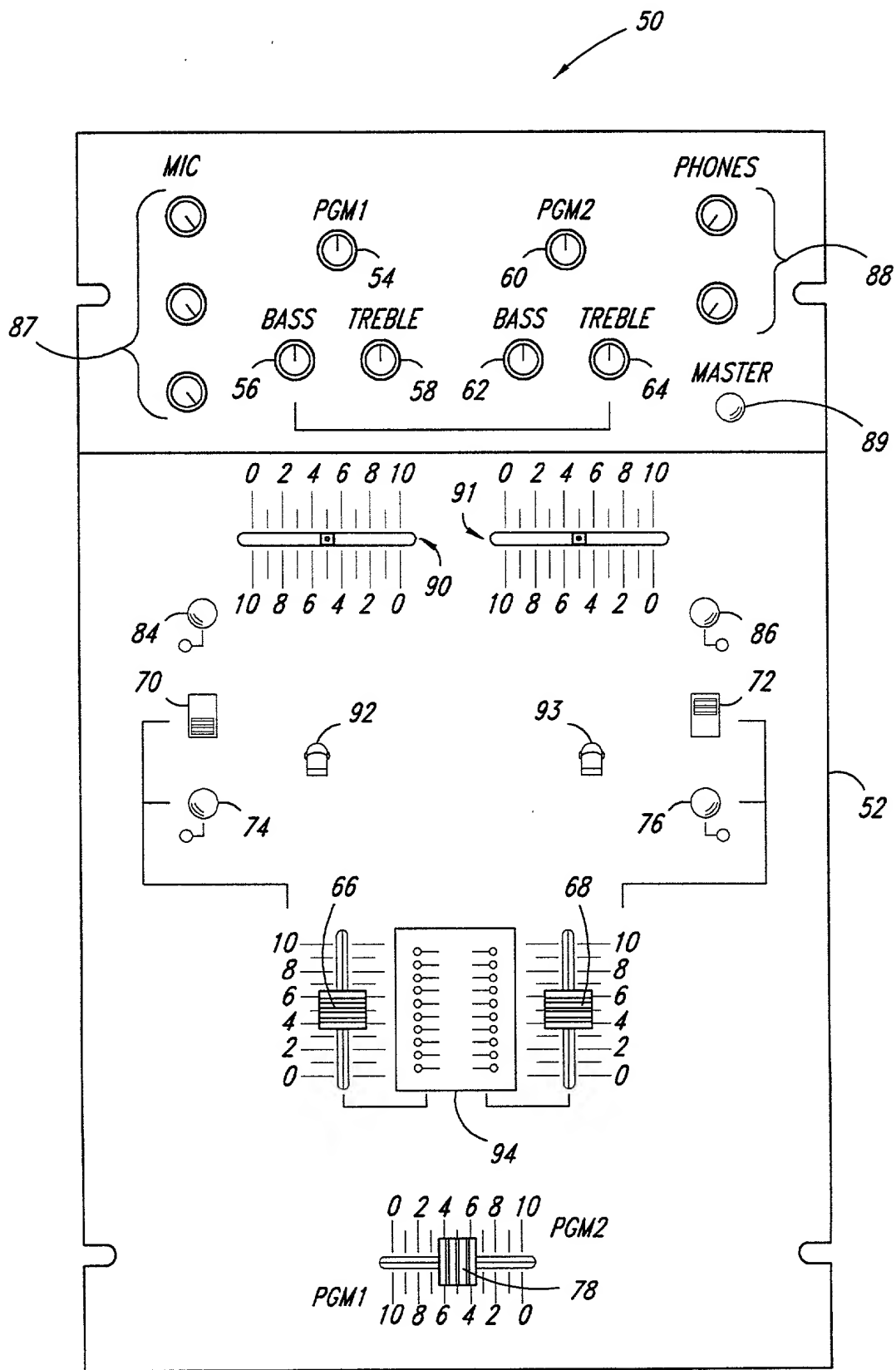


FIG. 5A

50

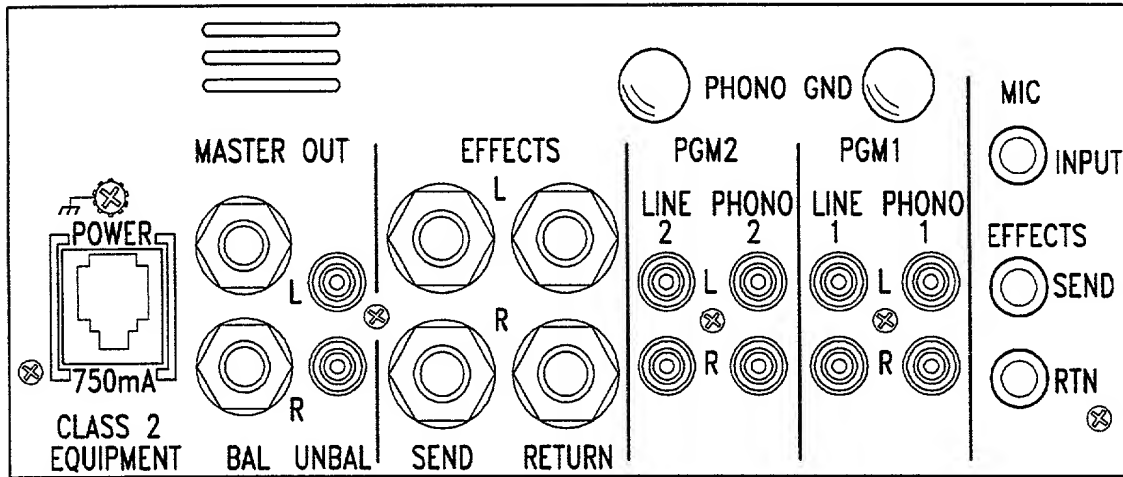


FIG. 5B

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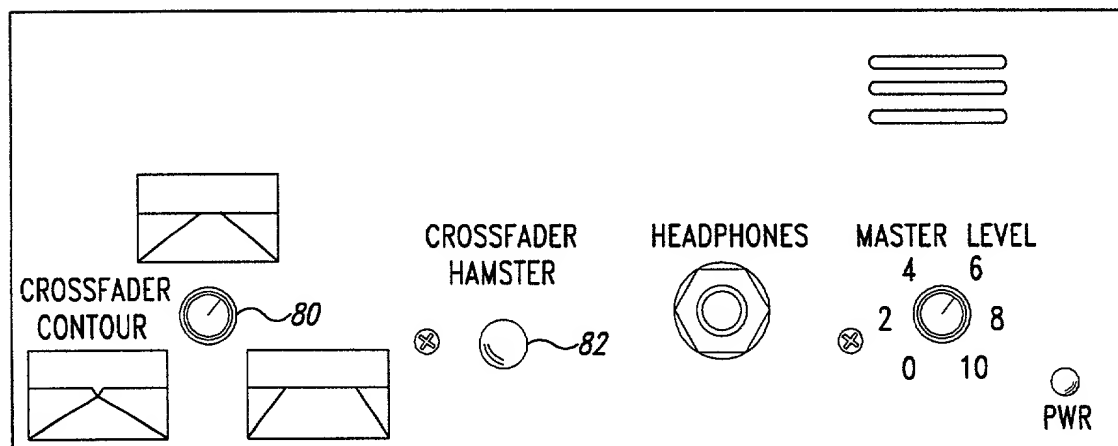


FIG. 5C

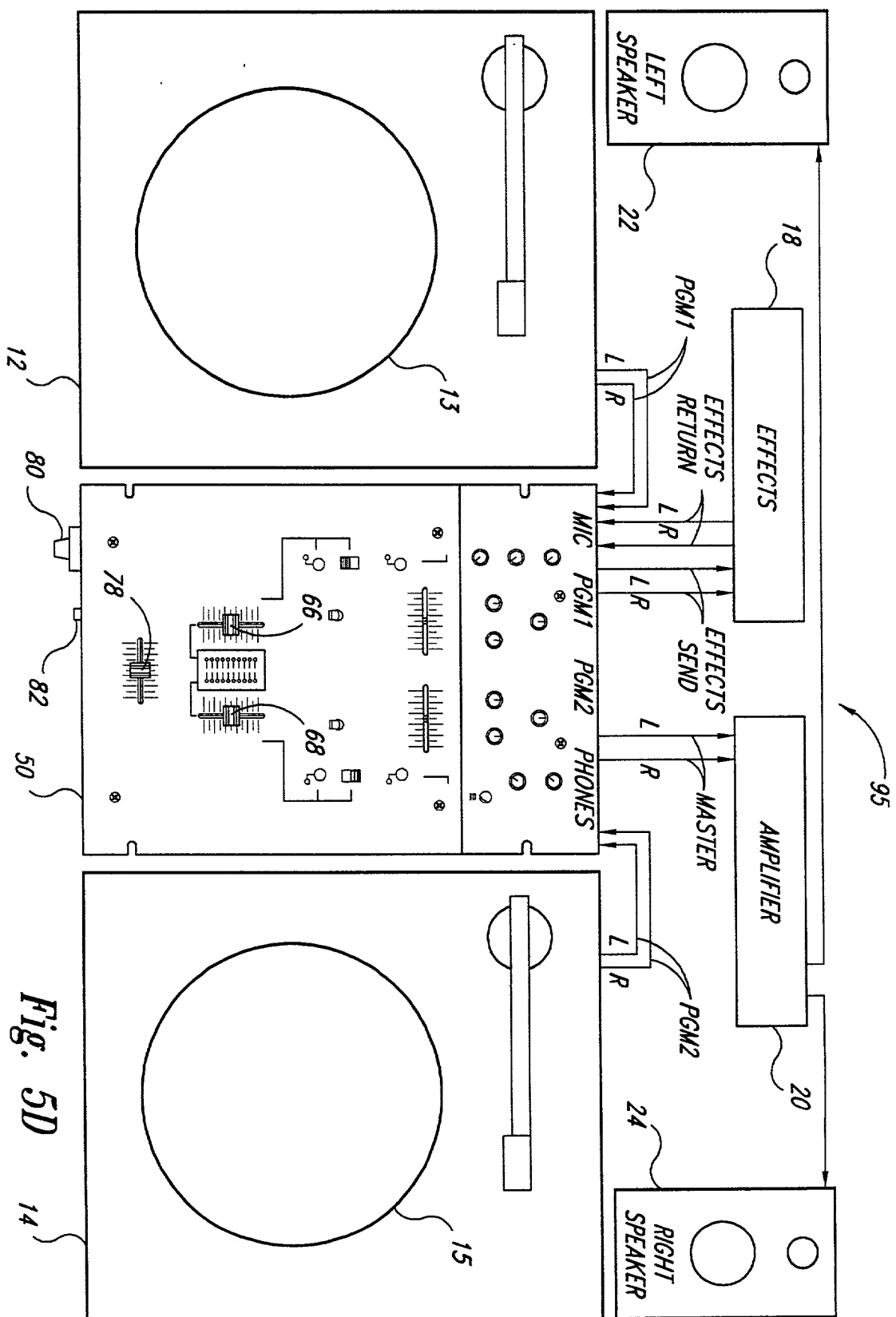


Fig. 5D¹⁴⁾

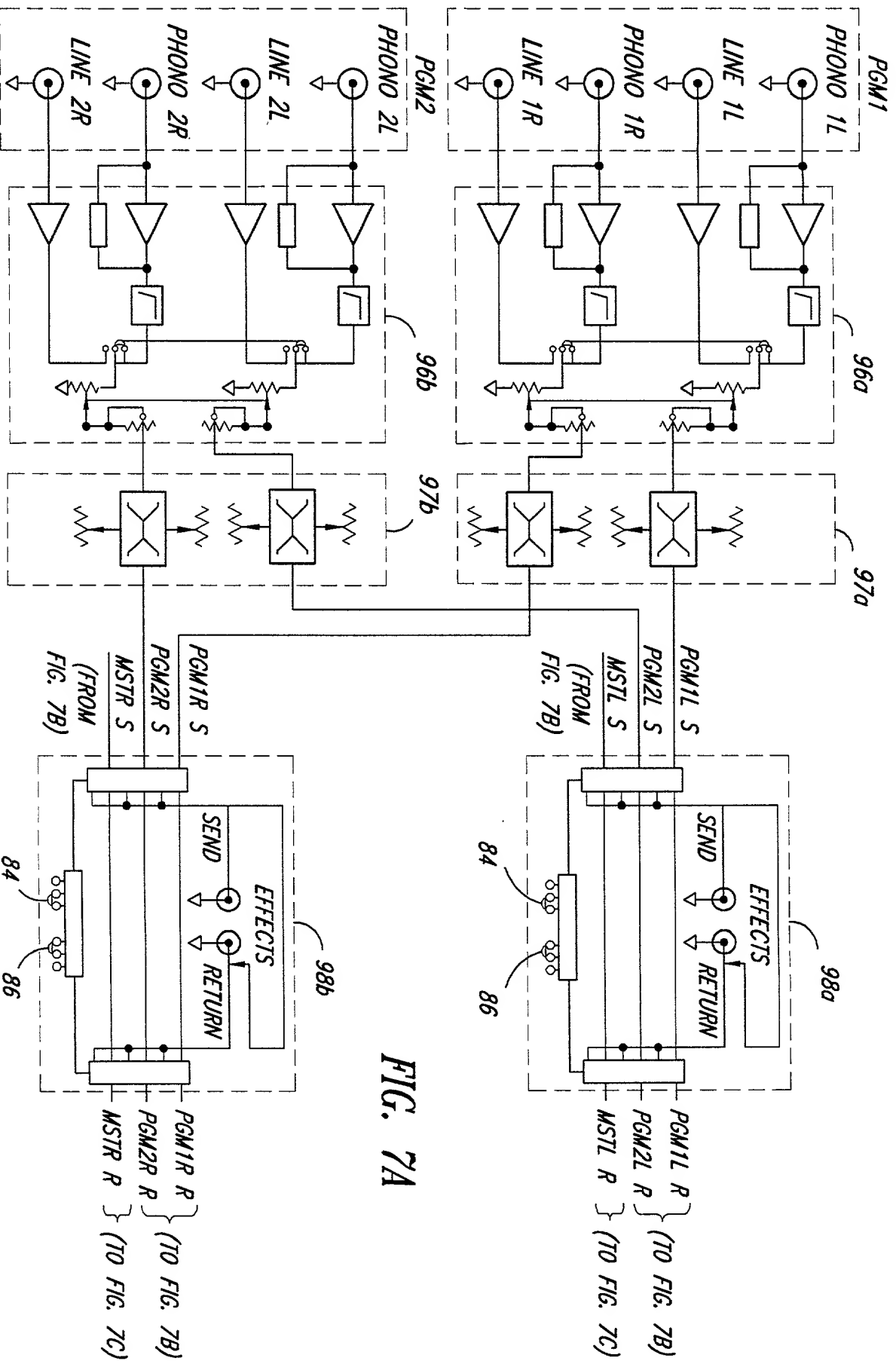


FIG. 7A

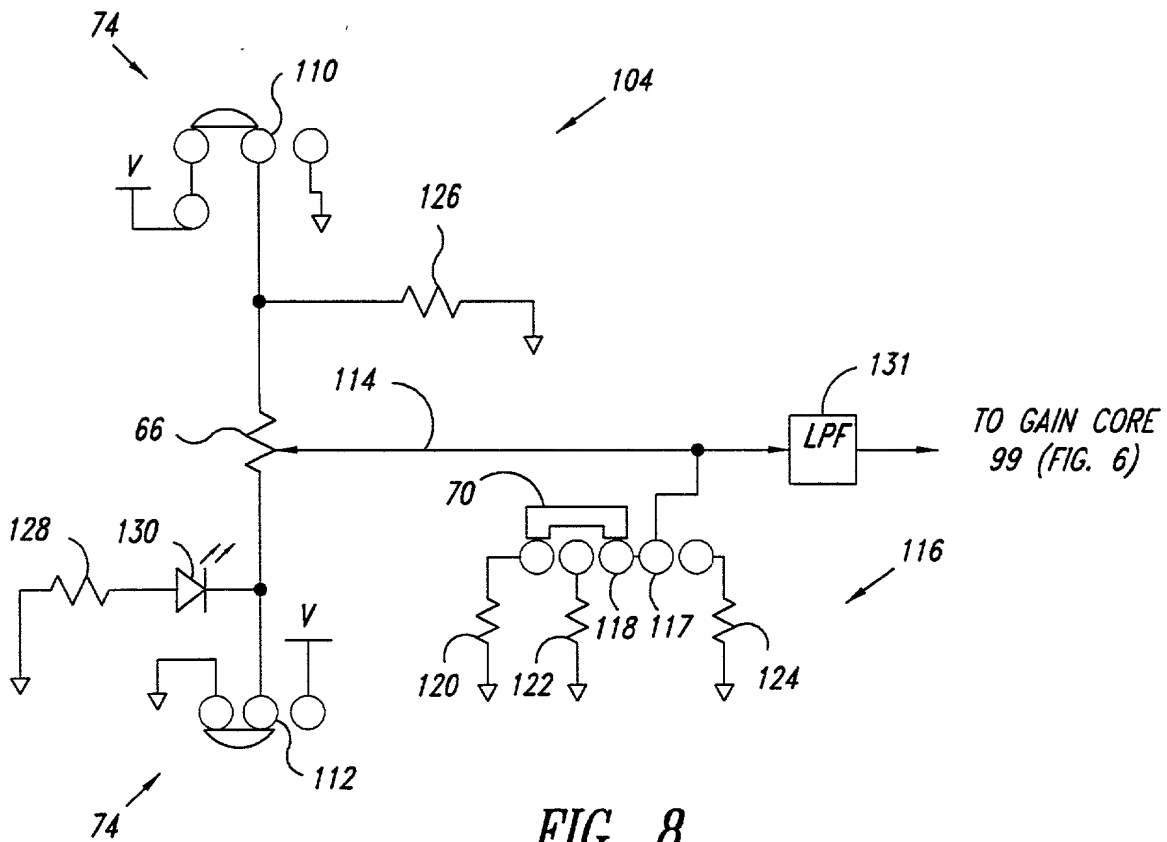


FIG. 8

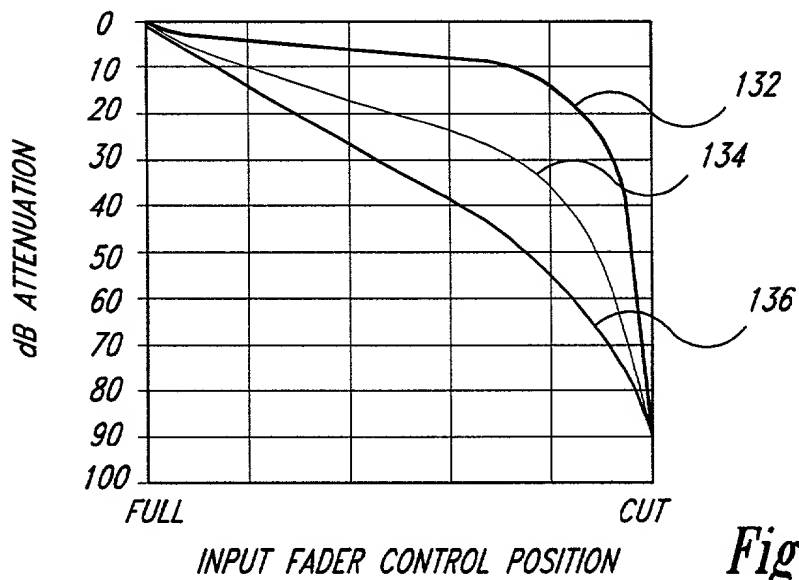


Fig. 9

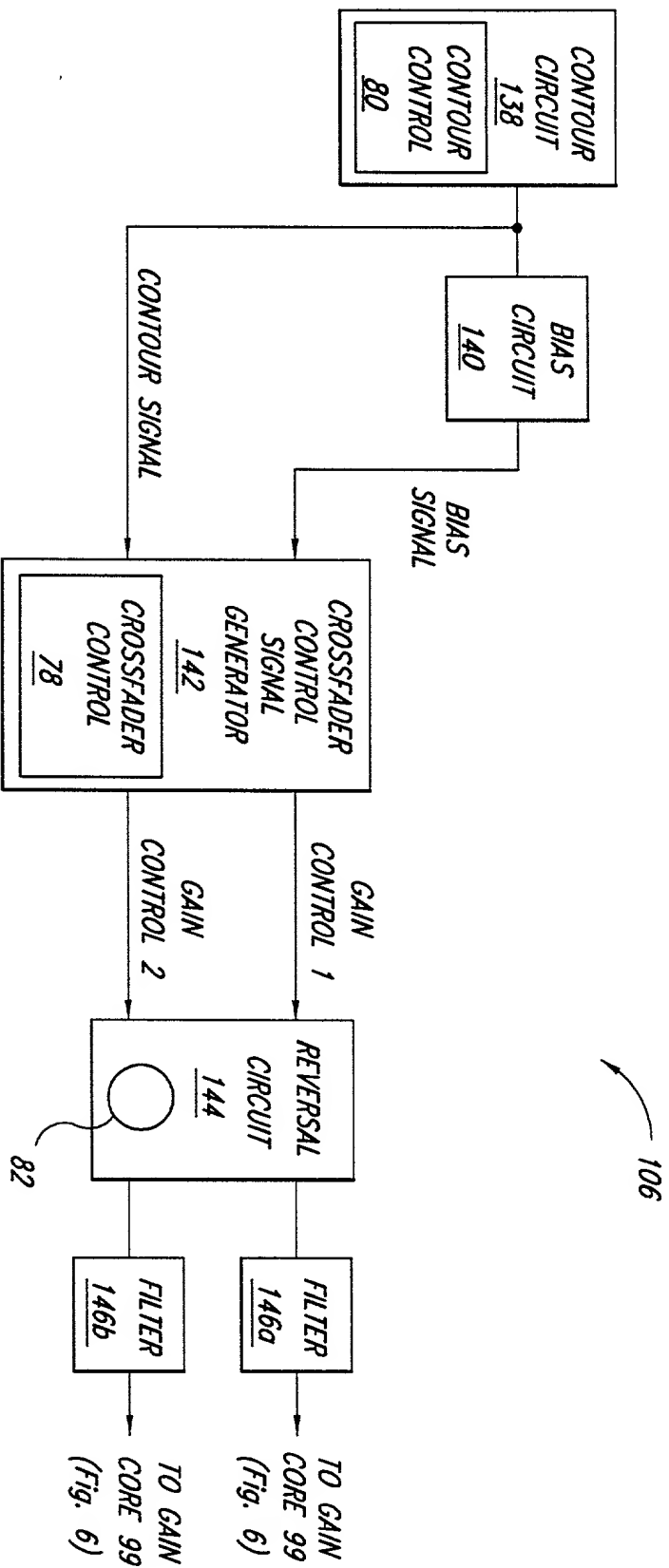


FIG. 10

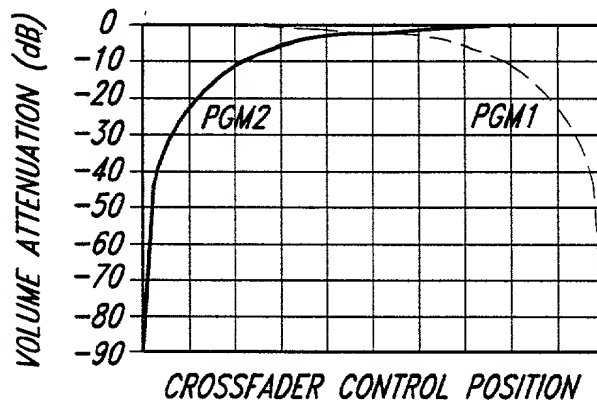


FIG. 11A

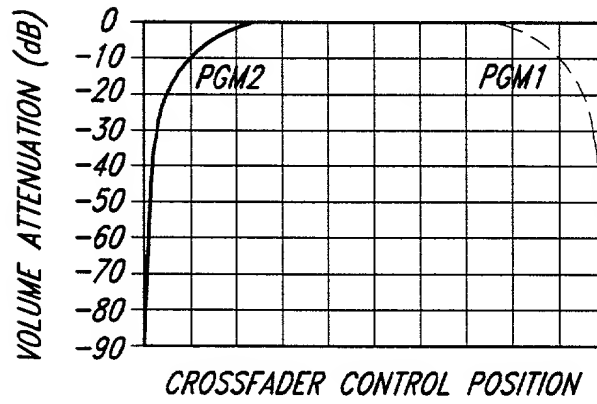


FIG. 11B

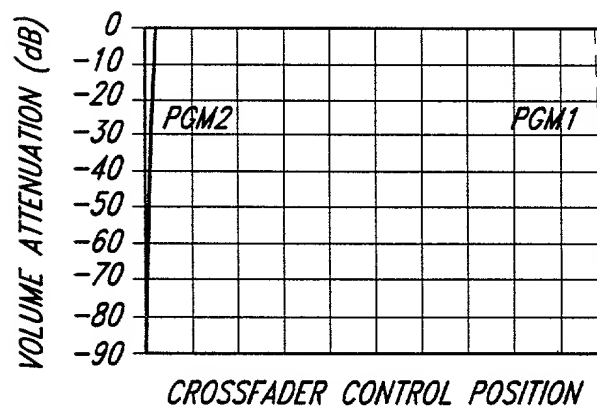


FIG. 11C

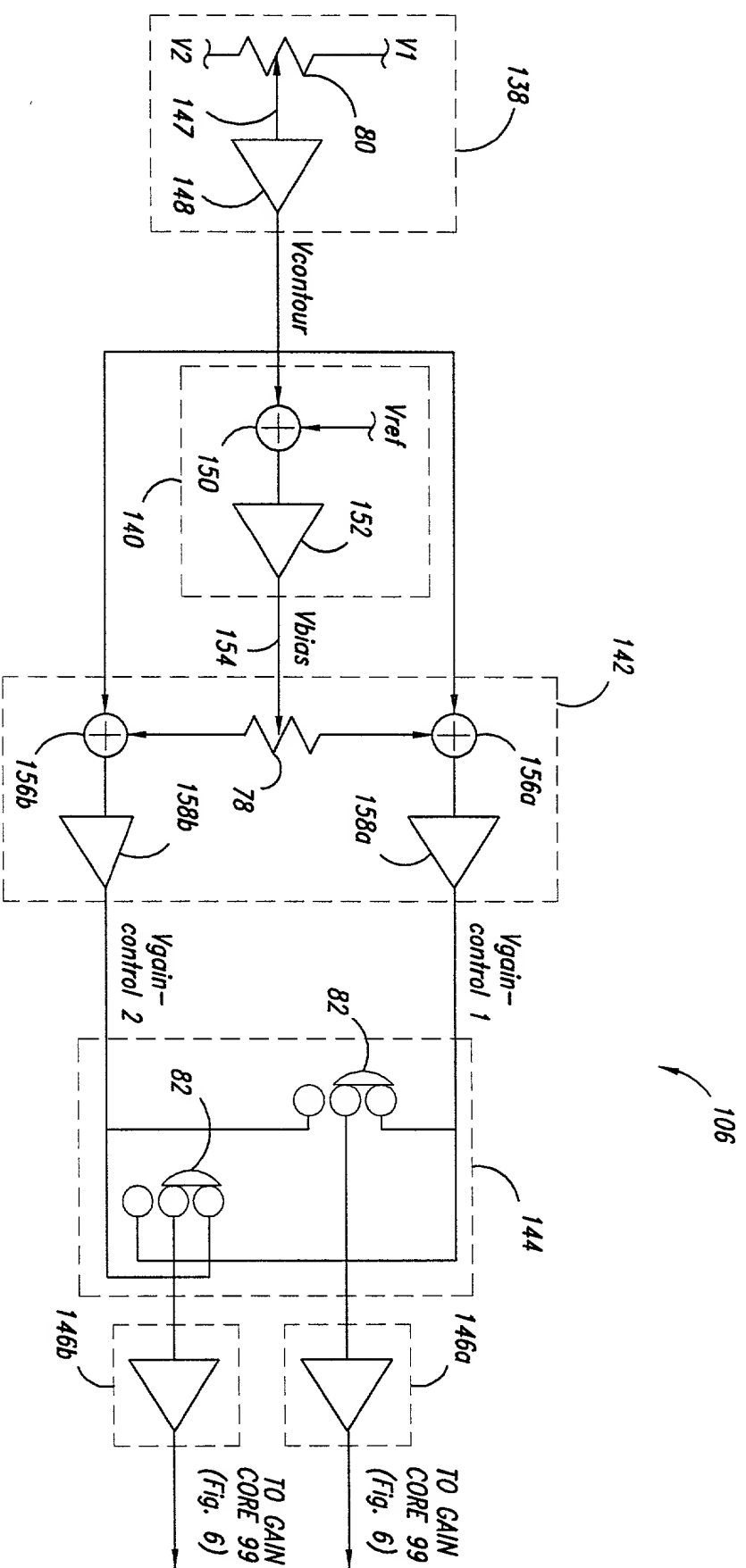


FIG. 12

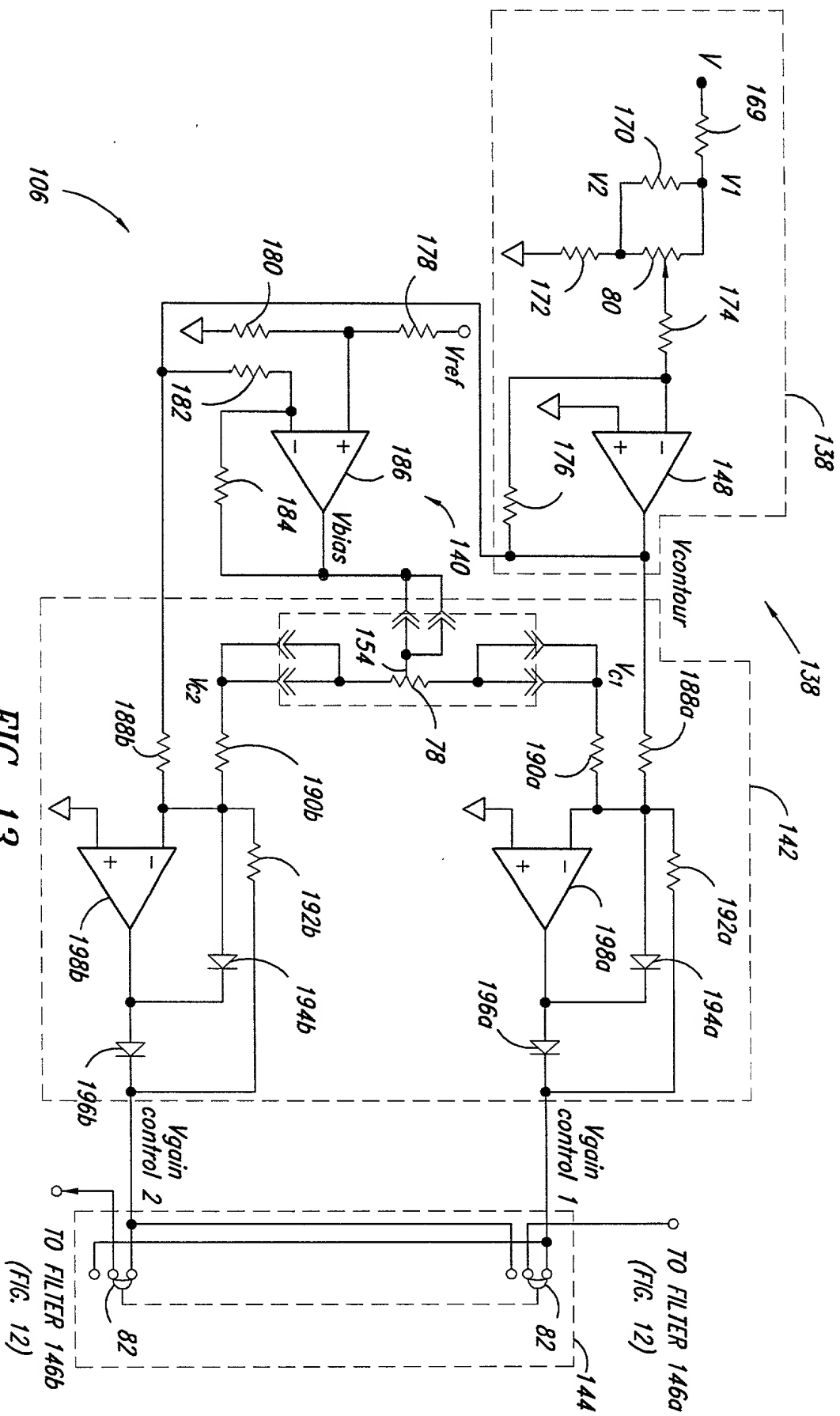


FIG. 13

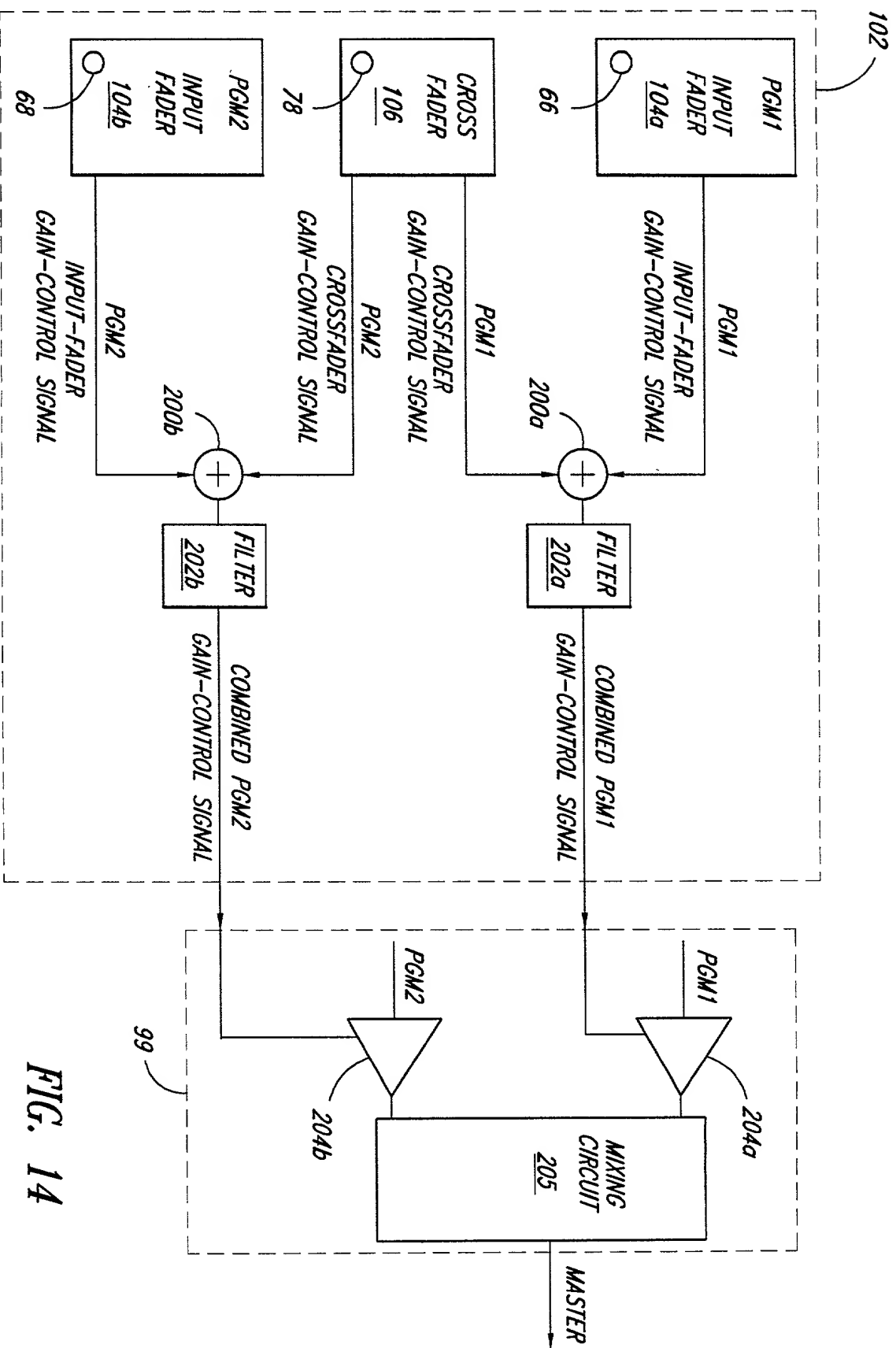


FIG. 14

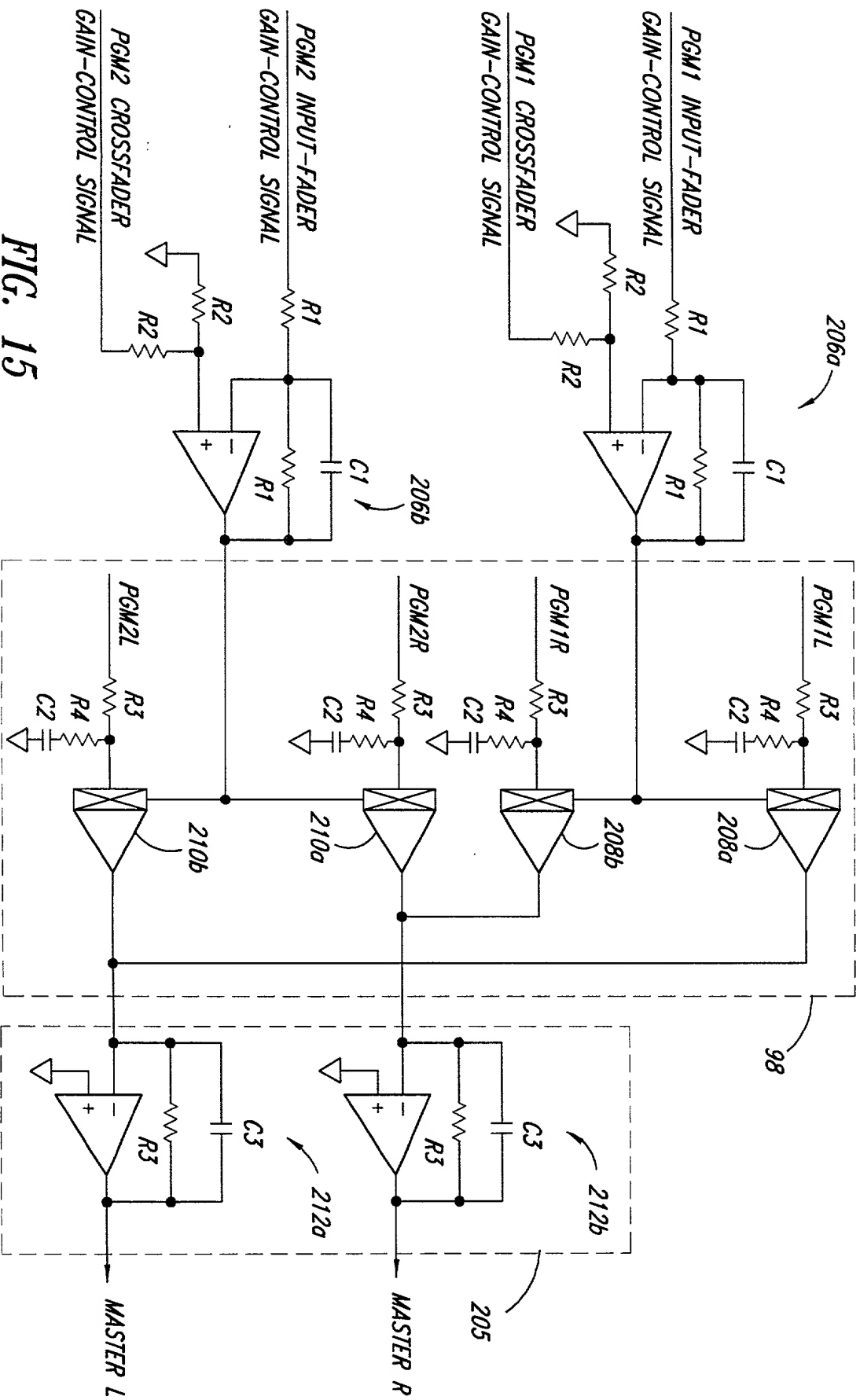
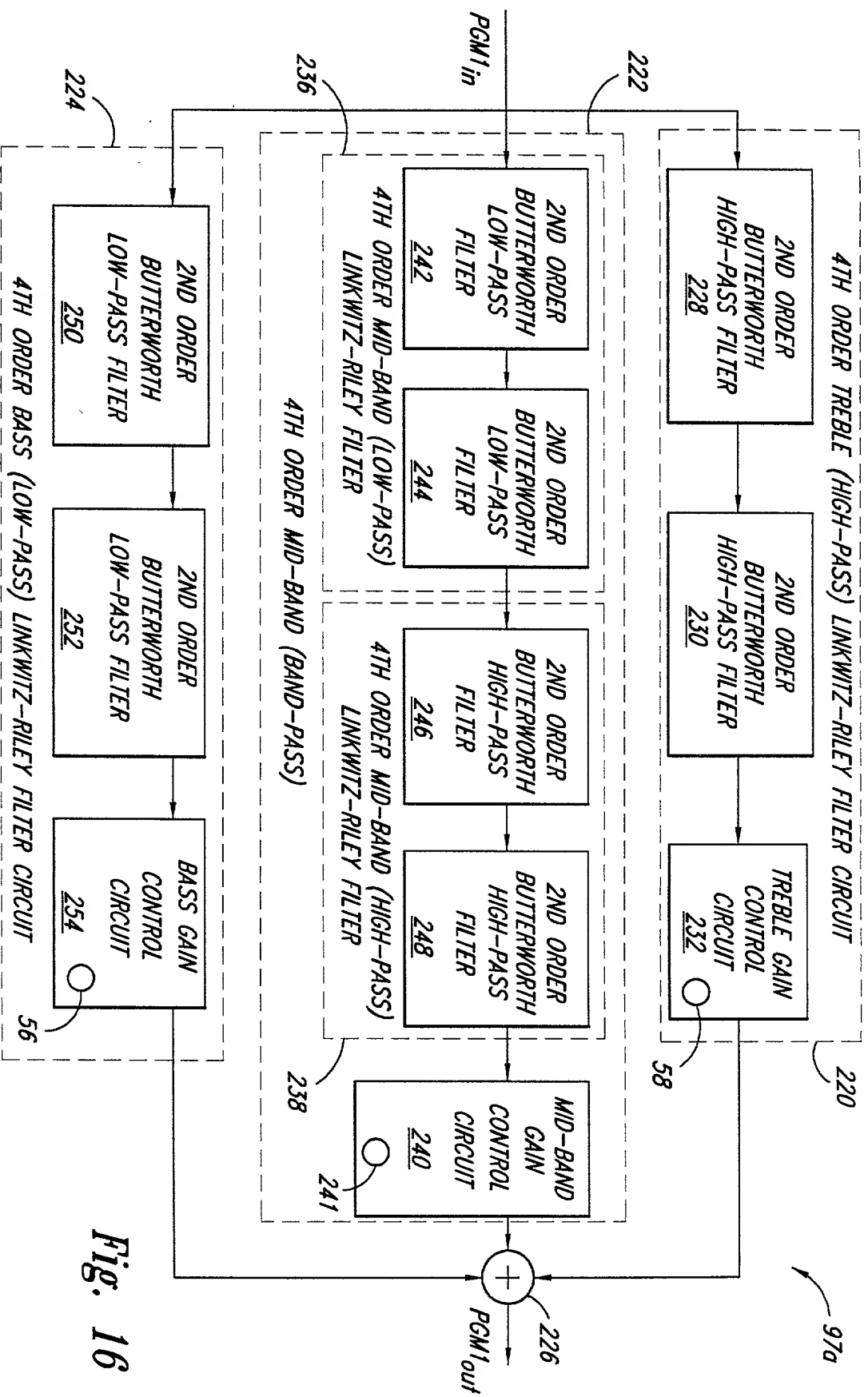


FIG. 15



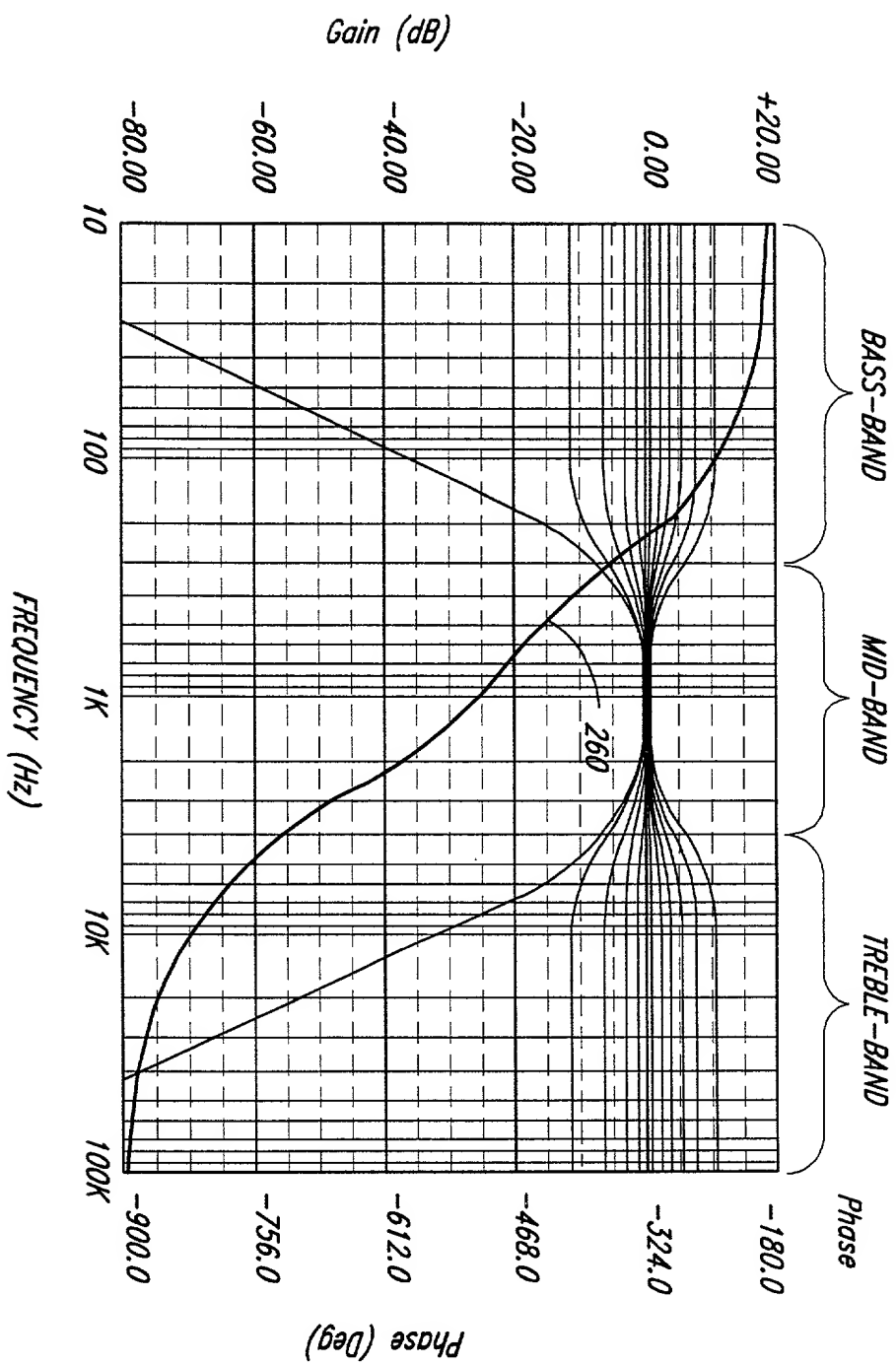


FIG. 17

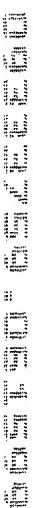
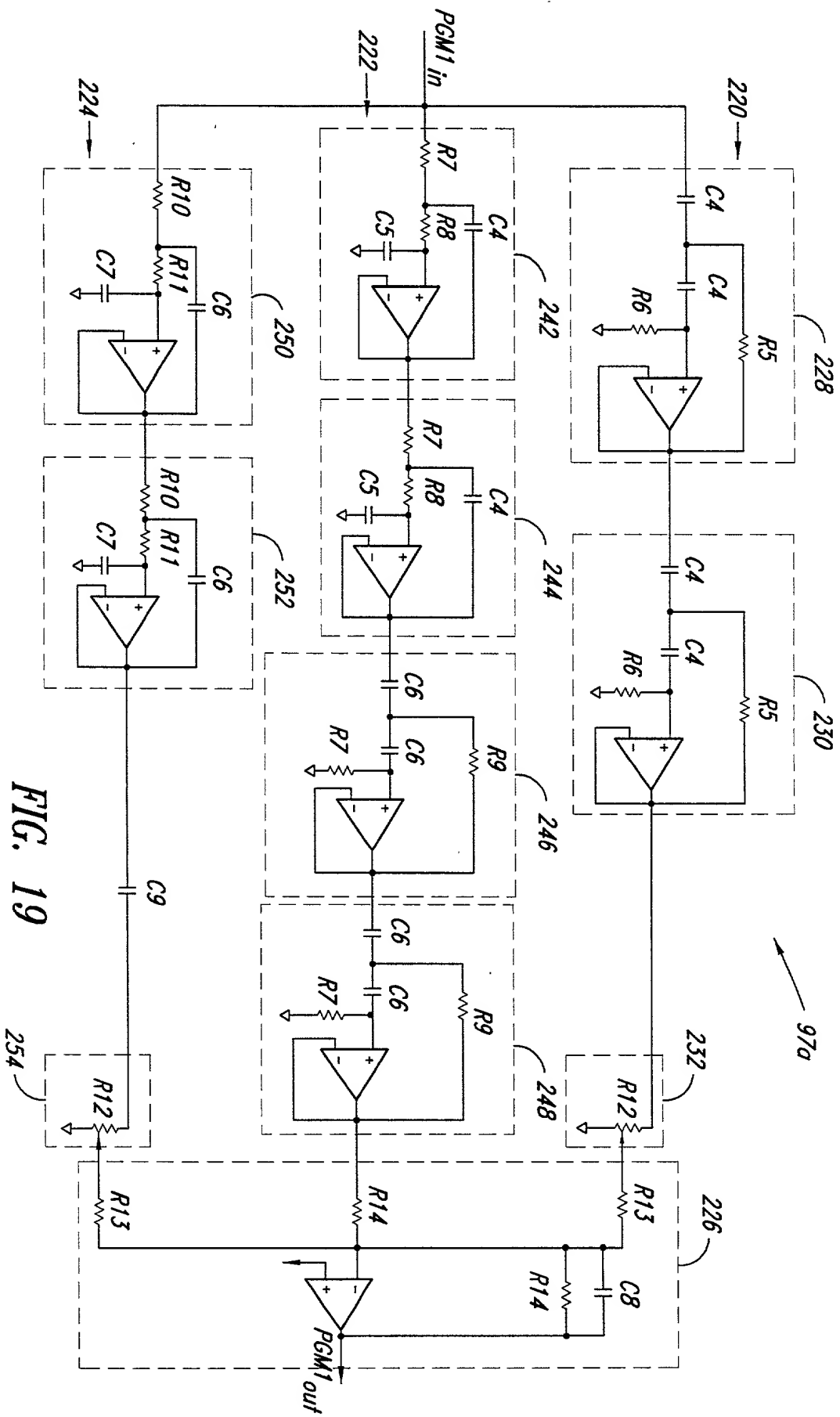


FIG. 18



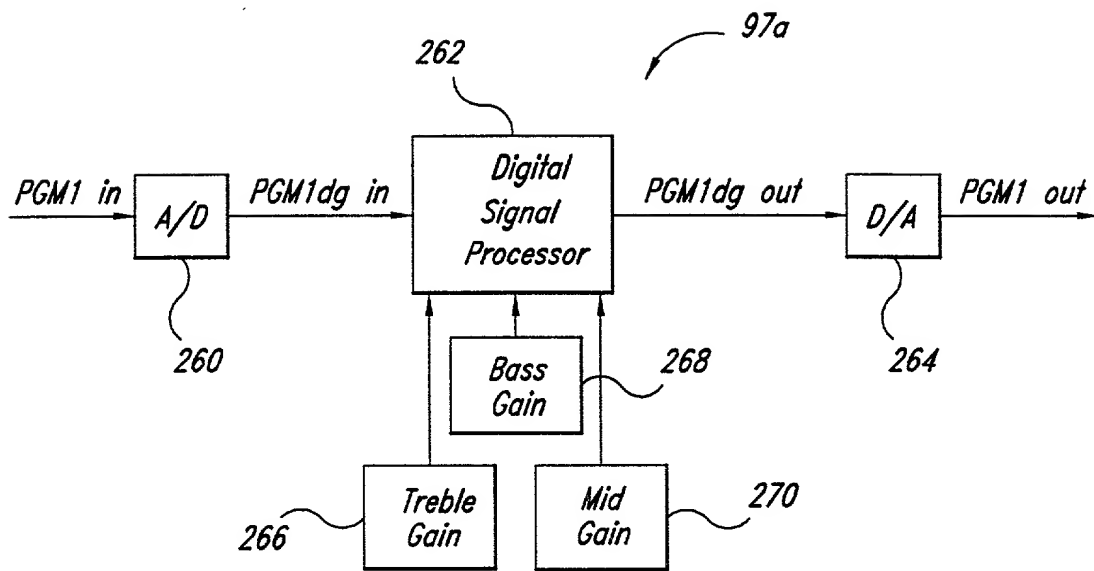


Fig. 20

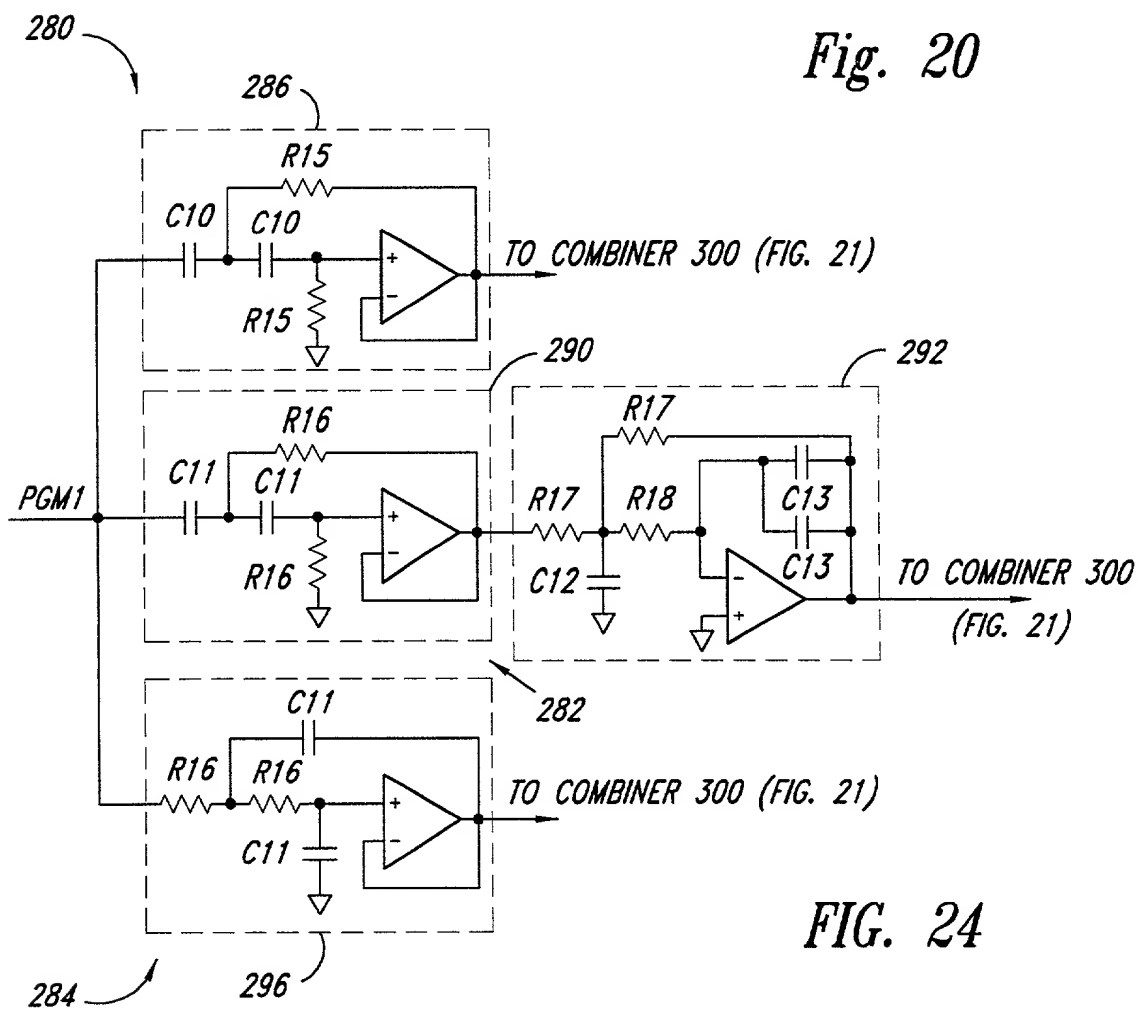


FIG. 24

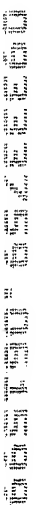


FIG. 22

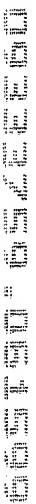
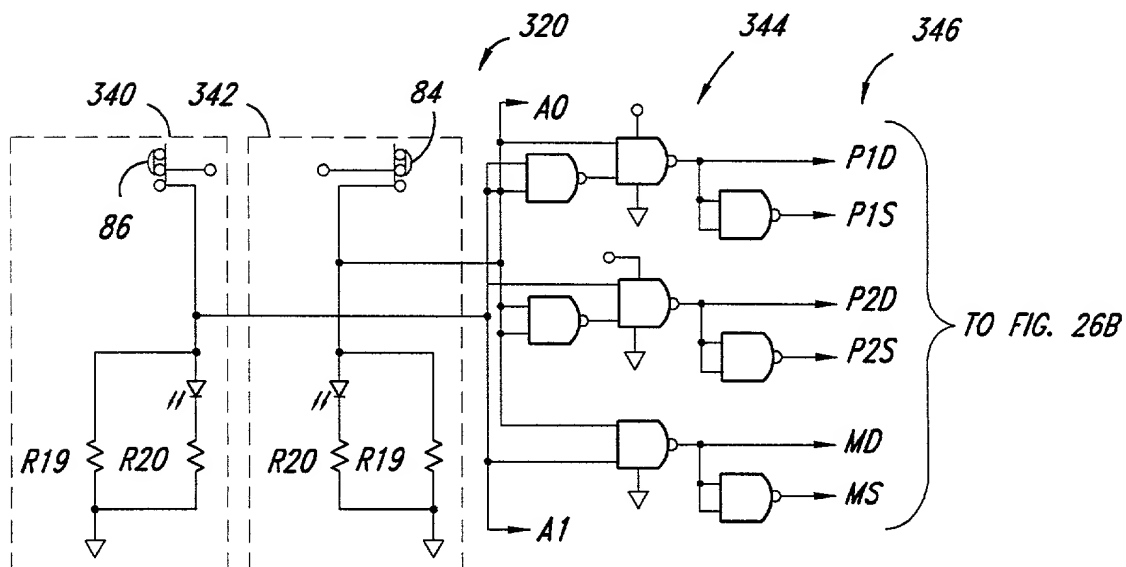
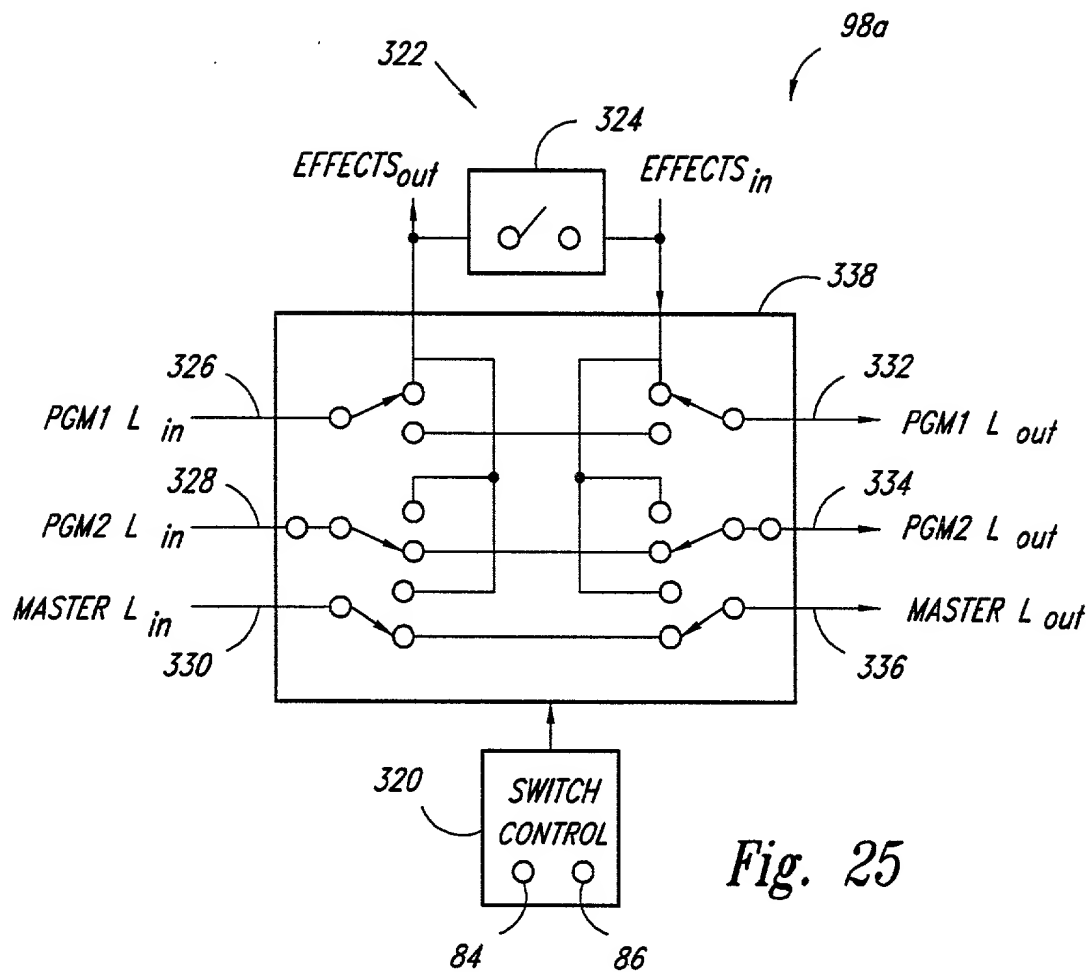


FIG. 23



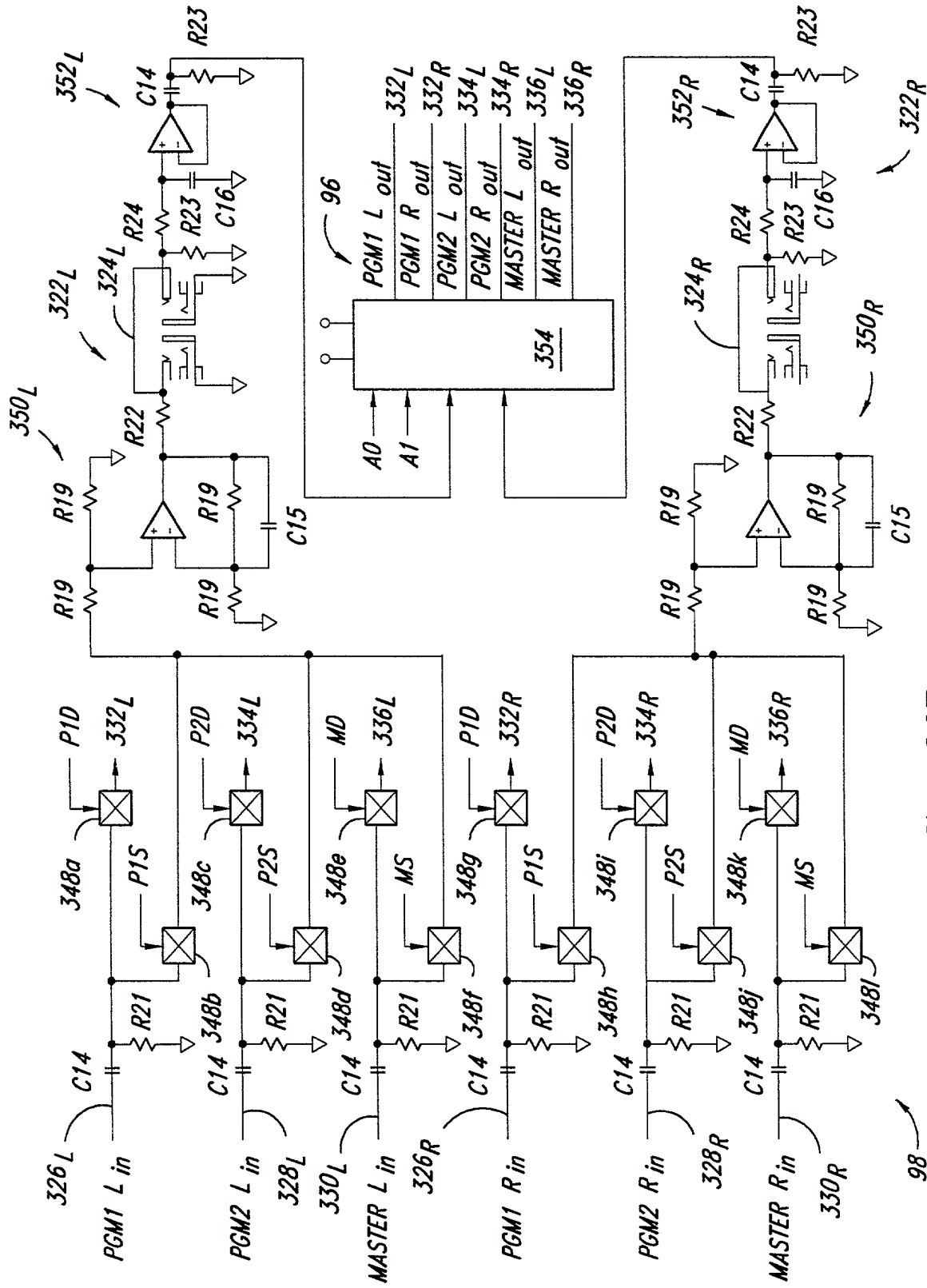


Fig. 26B

**DECLARATION AND POWER OF ATTORNEY
IN PATENT APPLICATION**

Attorney Docket No.: 35-28

As a below named inventor, I hereby declare:

My residence, post office address and citizenship are as stated below next to my name.

I believe that I am the original, first and sole inventor (if only one name is listed below) or a joint inventor (if plural inventors are listed below) of the subject matter that is claimed and for which a patent is sought on the invention entitled:

IMPROVED TONE-CONTROL CIRCUIT AND METHOD FOR CONDITIONING

RESPECTIVE FREQUENCY BANDS OF AN AUDIO SIGNAL

the specification of which

- ☒ is attached hereto.
- ☐ was filed on _____ as U.S. Application Serial No. (or PCT International Application No.) _____ and was amended on _____ (if applicable).

I hereby state that I have reviewed and understand the contents of the above-identified specification, including the claims, as amended by any amendment referred to above.

I acknowledge the duty to disclose information which is material to patentability as defined in Title 37, Code of Federal Regulations, Section 1.56.

I hereby claim foreign priority benefits under Title 35, United States Code, Section 119(a)-(d) or Section 365(b), of any foreign application(s) for patent or inventor's certificate, or Section 365(a) of any PCT international application designating at least one country other than the United States listed below and have also identified below any foreign application for patent or inventor's certificate having a filing date before that of the application on which priority is claimed.

Prior Foreign Application(s):

<u>Number</u>	<u>Country</u>	<u>Date Filed</u>	<u>Priority Claimed</u>
_____	_____	<u>Day/Mo/Year</u>	<u>Yes/No</u>
_____	_____	<u>Day/Mo/Year</u>	<u>Yes/No</u>

I hereby claim the benefit under Title 35, United States Code Section 119(e) of any United States provisional application(s) listed below.

<u>Application No.</u>	<u>Filing Date</u>
_____	_____

I hereby claim the benefit under Title 35, United States Code, Section 120 of any United States application(s), or Section 365(c) of any PCT international application designating the United States listed below, and, insofar as the subject matter of each of the claims of this application is not disclosed in the prior United States or PCT international application in the manner provided by the first paragraph of Title 35, United States Code, Section 112, I acknowledge the duty to disclose information which is material to patentability as defined in Title 37, Code of Federal Regulations, Section 1.56, which became available between the filing date of the prior application and the national or PCT international filing date of this application.

<u>Application Number</u>	<u>Filing Date</u>	<u>Status: Patented Pending/Abandoned</u>
_____	_____	_____
_____	_____	_____

I hereby appoint LARRY A. JACKSON, Reg. No. 24,313, JEFFREY T. HALEY, Reg. No. 34,834, STEPHEN M. EVANS, Reg. No. 37,128, BRYAN A. SANTARELLI, Reg. No. 37,560, and RICHARD O. GRAY, Reg. No. 26,550, of Graybeal Jackson Haley, LLP, 777 - 108th Avenue N.E., Suite 2460, Bellevue, Washington 98004-5117, as its attorneys to prosecute this application and to transact all business in the United States Patent and Trademark Office connected therewith.

Address all correspondence and phone calls to:

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777-108th Avenue NE, Suite 2460
Bellevue, WA 98004-5117
(425) 455-5575

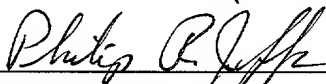
I hereby further declare that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under Section 1001 of Title 18 of the United States Code, and that such willful false statements may jeopardize the validity of the application or any patent issued thereon.

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Post Office Address (if different from Residence)


Inventor's Signature

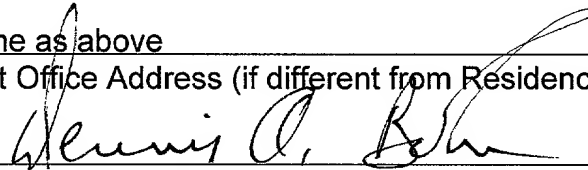
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Inventor's Signature

6-8-99
Date